

Characteristics dipole antenna for partial discharge in gas insulated switchgear

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ABSTRACT

The insulation condition of high-voltage equipment can be determined by measuring partial discharge (PD), which is an important indicator in insulation degradation. One of the PD detection methods that can be used is to use antennas as sensors in detecting electromagnetic waves generated from PD activities, especially in gas insulated switchgear (GIS) systems. This study focuses on designing and testing dipole antennas in the ultra-high frequency (UHF) frequency range of 300 Mhz-3 GHz to detect PD signals in GIS. Previous studies on dipole antennas with dimensions of 66×15 mm have reported a bandwidth of 336 MHz and a return loss of -22.4 dB at 1.3 GHz. The antenna was fabricated using an FR4-epoxy substrate with a thickness of 1.6 mm, a substrate radius of 102 mm, and a gap distance of 2 mm. Optimization of the antenna length and width significantly improved performance characteristics. Simulation results show that a dipole antenna with dimensions of 35×40 mm antenna produced a wider bandwidth of 989 MHz with a return loss of -28.47 dB at 1.4 GHz. Experimental validation using vector network analyzer (VNA) and PD testing on GIS confirmed that the optimized dipole antenna effectively detected PD activity at a voltage level of 16 kV.

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1. INTRODUCTION

The insulation condition of high-voltage equipment is commonly assessed through partial discharge measurements. Antenna sensors, which detect electromagnetic waves generated by partial discharge activity, are commonly used in gas-insulated switchgear [1], [2]. The range of frequency from 300 MHz to 3 GHz, classified as ultra-high frequencies (UHF), represents the electromagnetic wave signals utilized in GIS [3], [4]. Electromagnetic waves can be measured using UHF antennas [5]. Compared to gas sensors, UHF sensors in gas-insulated switchgear (GIS) offer faster response times and higher sensitivity [6]. The UHF method operates within a frequency range of 300 MHz to 3 GHz in GIS. An antenna designed for this frequency range effectively detects partial discharge, confirming its suitability for GIS monitoring.

UHF antennas employed as sensors for partial discharge (PD) detection must exhibit high sensitivity and a broad bandwidth. Furthermore, the antenna dimensions should correspond to the opening window in the GIS. Optimization of antenna design should consider the specific parameters required by the PD sensor [7].

Important parameters for antennas employed as sensors include bandwidth and return loss. Bandwidth is generally defined as the range of frequencies within the UHF band where the return loss (RL) value remains below -10 decibels (dB). This criterion is widely used for bandwidth calculation in most studies [8]-[13].

Antennas operate by receiving and transmitting electromagnetic signals. A dipole antenna features a symmetrical structure, with both sections exhibiting identical shapes and dimensions. The length and width of dipole antennas may be modified to accommodate particular applications.

The antenna design process typically begins with the use of three-dimensional modeling software, such as HFSS [14]. Subsequent stages involve testing with a vector network analyzer (VNA) and assessing the antenna's performance as a sensor for detecting partial discharge in GIS [15], [16]. In this study, dipole antennas were fabricated using three-dimensional modeling software, such as ANSYS HFSS, then tested with a VNA, and evaluated within GIS environments.

Dipole antennas are commonly employed to detect partial discharge [17]. A dipole antenna measuring 66 mm × 15 mm has previously been utilized to identify partial discharge in a 66 kV GIS model [18]. Table 1 shows the result of the dipole antenna at 66×15 mm.

Table 1. Simulated results of dipole antenna at 66×15 mm [18]

| Name of antenna | Return Loss (dB) | Fr (GHz) | Bandwidth (MHz) |
|-----------------|------------------|----------|-----------------|
| Dipole antenna | -22.4 | 1.3 | 336 |

Research on dipole antennas used as sensors has been limited. However, to date, dipole antennas have not been fabricated using three-dimensional modeling techniques that involve modifying antenna dimensions to optimize performance characteristics. The fabrication of dipole antennas with three-dimensional modeling aims to achieve optimal bandwidth, return loss, and resonance frequency, which are critical for effective partial discharge detection. In this context, the antenna's length and width are systematically varied to evaluate their impact on performance parameters.

2. OBJECTIVES

This study aims to design and analyze antennas operating within the 300 MHz to 3 GHz frequency range by varying key antenna parameters. Additionally, PD detection on GIS is evaluated using a dipole antenna as the sensor. This research contributes by proposing a method to determine optimal specifications for a dipole antenna, which has not been widely studied. Therefore, the author seeks to understand more deeply the changes that can be made to the dipole antenna's shape (length and width) to achieve the most effective antenna size. The determination of an antenna can be seen in its wide bandwidth, low return loss, and resonance frequency. Meanwhile, the antenna made is a microstrip patch antenna using FR4-epoxy substrate with a thickness of 1.6 mm, a substrate radius of 102 mm, and a gap distance of 2 mm.

3. METHOD

The fabrication of the dipole antenna begins with designing the antenna using three-dimensional modeling software. Following the identification of the optimal configuration, the antenna undergoes testing with a VNA. Subsequently, the antenna functions as a sensor for detecting partial discharge within the GIS [18]. The experimental procedure employed in this study is illustrated in Figure 1.

Figure 1 illustrates the methodology employed in this study. The process begins with specifying the desired antenna. First, a dipole antenna is designed as a microstrip patch antenna using an FR4-epoxy substrate with a thickness of 1.6 mm, a substrate radius of 102 mm, and a gap distance of 2 mm. Next, antenna simulations are conducted by varying the length and width parameters. Based on these simulation results, the optimal antenna is selected based on the criteria of wide bandwidth, low return loss, and resonant frequency. The selected antenna is then fabricated. After fabrication, a VNA is used to perform a measurement. Finally, the procedure concludes with PD testing, which represents the final stage of the research method.

A dipole antenna consists of two square plates arranged in series, each with identical dimensions and separated by a specified distance [19]. The square geometry is defined by its length (L) and width (W). Adjusting these parameters influences the resonance frequency, bandwidth, and return loss of the antenna.

The UHF response of dipole antennas is characterized by the following equations [18].

$$f_r = \frac{1}{2} \cdot k \cdot \frac{c}{l} \quad (1)$$

Where the f_r = resonant frequency of the antenna; k = constant 0.95; c = speed of light, 3×10^8 m/s; l = antenna length.

The expression for effective dielectric constant [20]:

$$\epsilon_{eff} = \frac{\epsilon_r + 1}{2} + \frac{(\epsilon_r - 1) \left(1 + 12 \frac{h}{W}\right)^{-1/2}}{2} \tag{2}$$

Where the ϵ_{eff} = effective dielectric constant; ϵ_r = dielectric coefficient; W = width of antenna; h = thickness of substrate.

The resonance frequency is given by [20].

$$f_r = \frac{c}{2(L + 2\Delta L)\sqrt{\epsilon_{eff}}} \tag{3}$$

Where, f_r = resonance frequency; c = speed of light, 3×10^8 m/s; L = length of antenna.

Dipole antennas are fabricated using three-dimensional imaging software. Figure 2 presents the results of the dipole antenna simulation.

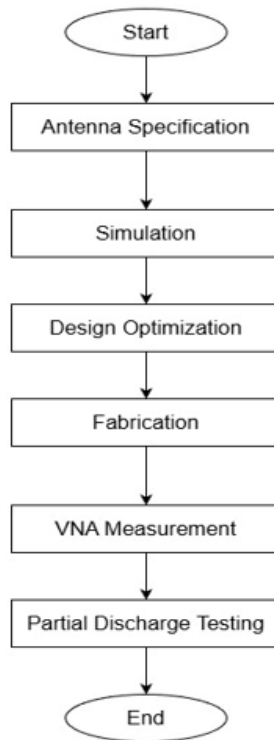


Figure 1. Research method flowchart

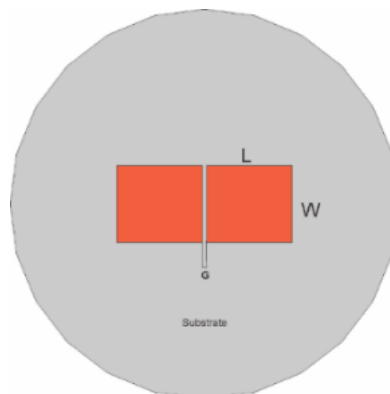


Figure 2. Dipole antenna configuration

Figure 2 illustrates the configuration of the dipole antenna. The performance of a dipole antenna is significantly influenced by its length and width. A gap exists between the two antenna elements, and a substrate serves as the material supporting the antenna patch. The primary design parameters in this study are the variations in width and length of the dipole antenna.

Following the simulation, the optimal antenna design is fabricated. To verify compliance with design specifications and optimal performance at the target frequency, the antenna is evaluated using a VNA. This evaluation measures electromagnetic characteristics, including return loss, resonance frequency, bandwidth, and antenna impedance. The Cobalt Series C1220 VNA, which operates over a frequency range of 100 kHz to 20 GHz, is utilized for these measurements.

The PD sensor testing on GIS evaluates the capabilities of the UHF dipole antenna, designed to detect PD events [21], [22]. The GIS model employs SF₆ insulation for high-voltage applications and features specifications including a voltage rating of 36 kV, a current rating of 2000 A, a transient current rating of 25 kA for 3 seconds, and a gas pressure rating of 0.75 kgf/cm² [23], [24]. The model includes two circular windows, each with a diameter of 50 mm, for the placement of external sensors. A conductive shield within the GIS prevents electromagnetic waves from escaping. However, the presence of a window with insulating material allows signals from PD sources to be detected by external sensors. The dipole antenna is positioned outside the GIS, in close proximity to the GIS window.

4. RESULTS AND DISCUSSION

The following section presents the results of modifications to the dipole antenna's length and width, as well as the outcomes of antenna and PD sensor tests on the GIS.

4.1. Dipole antenna characteristics

The performance of a dipole antenna is significantly affected by its length and width. A gap exists between the two sections of the antenna, and a substrate supports the antenna patch [25]. This design specifically examines variations in the width and length of the dipole antenna.

4.1.1. Dipole antenna width change

In the width change, there are eight simulated sizes, including (D × L): 45×25 mm, 45×30 mm, 45×35 mm, 45×40 mm, 45×45 mm, 45×50 mm, 45×55 mm, and 45×60 mm. The Figure 3 shows the dipole antenna with Figure 3(a) sizes 45×30 mm and Figure 3(b) sizes 45×60 mm.

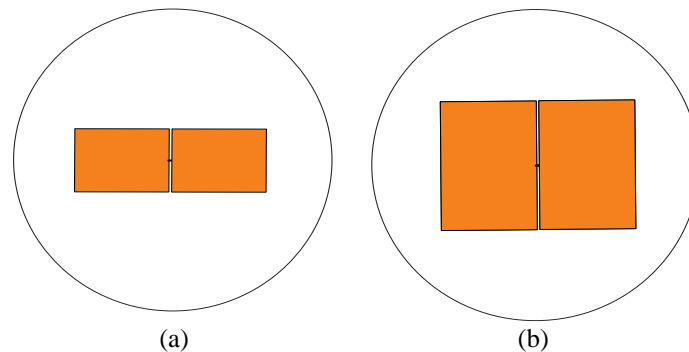


Figure 3. Dipole antenna (a) 45×30 mm and (b) 45×60 mm

For the width variation simulations, the following parameters were held constant: a FR4-epoxy substrate with a thickness of 1.6 mm, a substrate radius of 102 mm, a gap distance of 2 mm, and an antenna length of 45 mm. The simulation results for the effect of width variation on dipole antenna characteristics are presented in Table 2.

Simulation results for varying dipole antenna widths indicated that the configuration with the widest bandwidth, 819 MHz, occurred at a width of 45 mm and a length of 40 mm, accompanied by a return loss of -28.21 dB. For the voltage standing wave ratio (VSWR) simulation, the three optimal configurations were selected based on return loss and bandwidth: 45×35 mm, 45×40 mm, and 45×45 mm. The results of the top three impedance simulations for dipole antenna width variations are presented in Table 3.

Table 2. Simulated results of dipole antenna width variation on antenna characteristics

| Size length × width (mm) | Return loss (dB) | Fr (GHz) | Bandwidth (MHz) |
|--------------------------|------------------|----------|-----------------|
| 45×25 | -22.81 | 1.2 | 368 |
| 45×30 | -25.04 | 1.2 | 481 |
| 45×35 | -25.30 | 1.2 | 619 |
| 45×40 | -28.21 | 1.3 | 819 |
| 45×45 | -23.15 | 1.3 | 784 |
| 45×50 | -17.32 | 1.3 | 585 |
| 45×55 | -15.22 | 1.3 | 515 |
| 45×60 | -14.35 | 1.3 | 459 |

Table 3. Impedance simulation results for the three optimal dipole antenna width configurations

| Size length×width (mm) | The impedance values for these configurations are close to 50 Ohms | | |
|------------------------|--|-------------------|-------------------|
| | Frequency 1 (GHz) | Frequency 2 (GHz) | Frequency 3 (GHz) |
| 45×30 | 0.803 | 1.7 | 3.1 |
| 45×40 | 1.3 | 1.6 | 2.9 |
| 45×45 | 0.7 | 0.76 | 2.7 |

The VSWR is a parameter used to assess the degree of impedance matching between an antenna and the connected radio or transmission line. A VSWR value less than 2 is generally considered the standard for acceptable impedance matching 8,9,10,11,12,13. The three most effective impedance simulations demonstrate that varying the width of the dipole antenna produces three distinct operating frequencies with impedance values near 50 Ohms. According to the table, a dipole antenna measuring 45×30 mm achieves an impedance of 50 Ohms at 0.803 GHz, 1.7 GHz, and 3.1 GHz. For a dipole antenna sized 45×40 mm, the 50 Ω impedance occurs at 1.3 GHz, 1.6 GHz, and 2.9 GHz. In contrast, the 45×45 mm dipole antenna reaches 50 Ohms at 0.7 GHz, 0.76 GHz, and 2.7 GHz.

4.1.2. Dipole antenna length change

Six simulated dipole antenna sizes were evaluated for length variation, specifically (D × L): 25×40 mm, 30×40 mm, 35×40 mm, 40×40 mm, 45×40 mm, and 50×40 mm. In these simulations, the following parameters were held constant: FR4-epoxy substrate thickness of 1.6 mm, substrate radius of 102 mm, gap distance of 2 mm, and width of 40 mm. Figure 4 shows the sizes of 25×40 mm and 50×40 mm. The simulation results illustrating the effect of length variation on dipole antenna characteristics are presented in the Table 4.

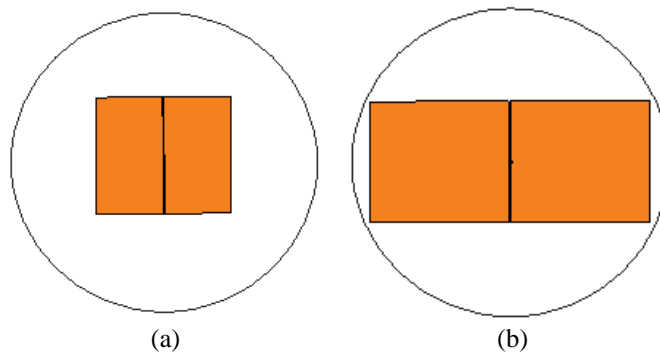


Figure 4. Dipole antenna (a) 25×40 mm and (b) 50×40 mm

Table 4. Simulation results for the effect of dipole antenna length variation on antenna characteristics

| Size: length×width (mm) | Return loss (dB) | Frequency (GHz) | Bandwidth (MHz) |
|-------------------------|------------------|-----------------|-----------------|
| 25×40 | -22.06 | 1.3 | 436 |
| 30×40 | -23.94 | 1.4 | 840 |
| 35×40 | -28.47 | 1.4 | 989 |
| 40×40 | -25.40 | 1.5 | 853 |
| 45×40 | -28.21 | 1.3 | 819 |
| 50×40 | -22.26 | 1.1 | 598 |

Simulation of dipole antenna length variations indicated that the 35×40 mm configuration achieved a minimum return loss of -28.47 dB at a resonance frequency of 1.4 GHz and a bandwidth of 989 MHz. For the voltage standing wave ratio (VSWR), values below 2 were observed for dipole antennas with dimensions of 30×40 mm, 35×40 mm, and 40×40 mm. The results of the three optimal impedance simulations for variations in dipole antenna length are presented in Table 5.

The data indicate that a dipole antenna measuring 30×40 mm exhibits an impedance of 50 ohms at 0.845 GHz. For a dipole antenna with dimensions of 35×40 mm, the 50-ohm impedance occurs at 0.846 GHz and 3 GHz. In contrast, the 45×40 mm dipole antenna achieves a 50-ohm impedance at 0.767 GHz, 1.6 GHz, and 2.932 GHz.

Based on variations in length and width, the three most effective antenna designs were selected. The optimal antenna simulations correspond to dimensions of 35×40 mm, 45×40 mm, and 45×45 mm.

Table 5. Simulation results for the three optimal dipole antenna length variations based on impedance performance

| Size length×width (mm) | Impedance values that have a value close to 50 Ohms | | |
|------------------------|---|-------------------|-------------------|
| | Frequency 1 (GHz) | Frequency 2 (GHz) | Frequency 3 (GHz) |
| 30×40 | 0,845 | | |
| 35×40 | 0,846 | 3 | |
| 45×40 | 0,767 | 1,6 | 2,932 |

4.2. Dipole antenna simulation analysis

The performance of a dipole antenna is determined by parameters such as its width and length. This section presents an analysis of simulation results examining how variations in these dimensions affect the antenna's characteristics.

4.2.1. The effect of width variation

The width of the dipole antenna was varied in simulations from 45×25 mm to 45×60 mm, with increments of 5 mm between each configuration. Figure 5 shows how differences in antenna width affect the results. Specifically, Figure 5(a) presents the return loss values resulting from changes in width, while Figure 5(b) presents the bandwidth gain resulting from these changes. This sequence illustrates the impact of antenna width on both return loss and bandwidth gain.

As the width of the dipole antenna increases, the minimum return loss value also increases. The relationship between width and bandwidth is non-linear, with bandwidth exhibiting fluctuations as width changes. Optimal bandwidth and return loss are achieved at dimensions of 45 mm by 40 mm, indicating that the dipole antenna performs best at these specific widths.

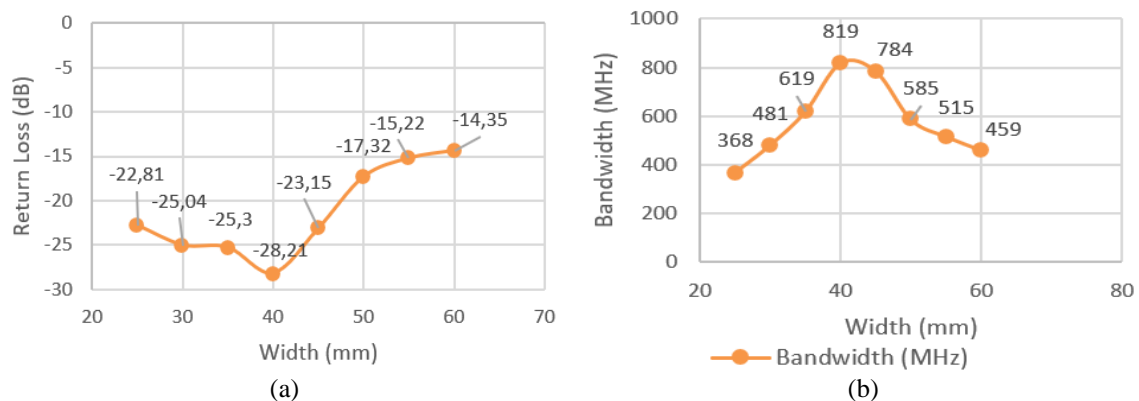


Figure 5. Comparison of width variations on (a) return loss and (b) bandwidth

4.2.2. The effect of length variation

On dipole antennas, the simulation of length changes used is from 25×40 mm to 50×40 mm. Changes in antenna length, made from one size to the next size by 5 mm. Figure 6 demonstrates the impact of varying antenna length in three stages. Figure 6(a) presents the return loss for different lengths. Figure 6(b)

depicts the resonant frequency as a function of antenna length. Figure 6(c) illustrates the variation in bandwidth with respect to antenna length.

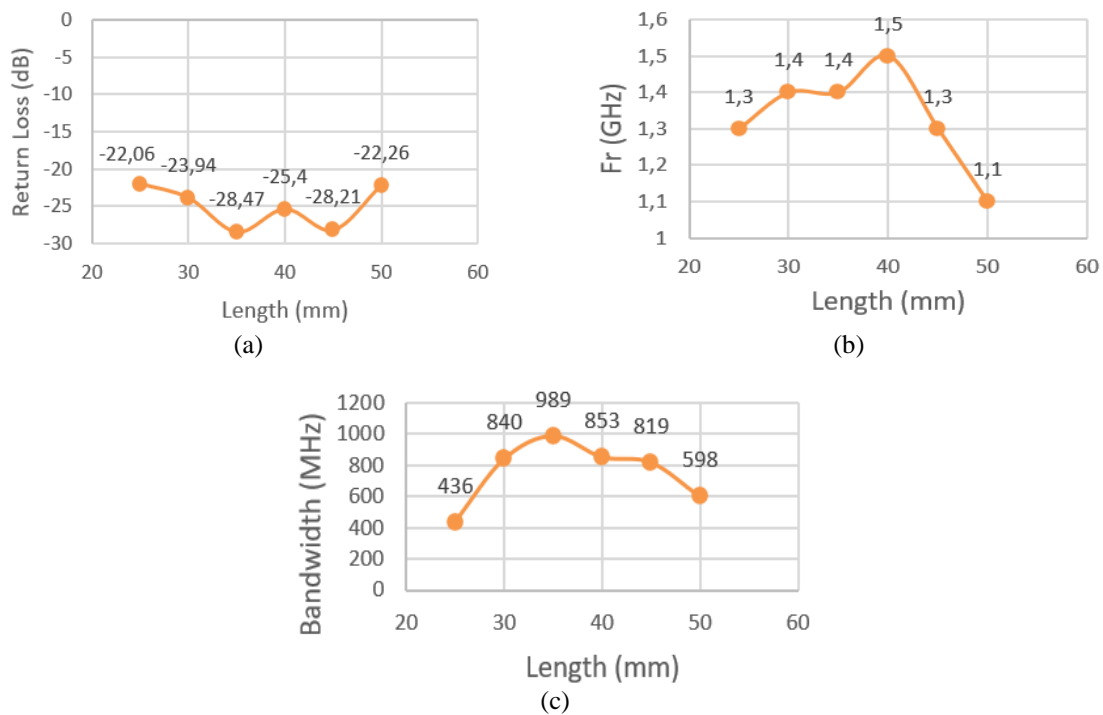


Figure 6. Comparison of the effects of length variation on (a) return loss, (b) resonance frequency, and (c) bandwidth

As the length of the dipole antenna increases, the resonance frequency decreases. Additionally, greater antenna length results in improved minimum return loss values. However, the bandwidth becomes more variable with increased length, with some lengths yielding larger bandwidths and others smaller. The UHF frequency response of a dipole antenna is determined by (1). By substituting different length values, such as 25 mm, 35 mm, and 45 mm, the following calculation results are obtained. Table 6 presents the results of simulations and calculations for antenna sizes of 25 mm, 35 mm, and 45 mm.

The results indicate that increasing the length of the dipole antenna leads to a decrease in the resonance frequency. Although the calculated and simulated values differ significantly, both methods demonstrate the same underlying principle: a longer dipole antenna produces a lower resonance frequency.

Optimizing dipole antenna performance requires adjusting its length. Reducing the antenna length increases the bandwidth, while increasing the length decreases the resonance frequency and reduces the return loss. Therefore, careful modification of the antenna length is essential to achieve the desired performance characteristics.

Table 6. Simulation and calculation results for variations in antenna length

| Size length (mm) | Resonance frequency (GHz) | |
|------------------|---------------------------|-------------|
| | Simulation | Calculation |
| 25 | 1,3 | 5,7 |
| 35 | 1,4 | 4,07 |
| 45 | 1,3 | 3,16 |

4.3. PD measurement results on GIS

Based on variations in length and width, the three most effective antennas were selected: 35×40 mm, 45×40 mm, and 45×45 mm. For the PD measurement in GIS, a dipole antenna with dimensions of 45×45 mm was utilized. PD test on solid insulation is one of the methods that determine the quality of insulation [26].

4.3.1. PDIV measurement

Partial discharge inception voltage (PDIV) is defined as the voltage at which partial discharge (PD) is first observed during the experiment. The voltage is gradually increased from a level where no PD is detected until PD appears. Measuring PDIV provides a reference for the minimum source voltage required to initiate PD in the test object. In this study, PDIV measurements were conducted using both the antenna sensor and the RC detector. Table 7 shows the results of the negative and positive PDIV tests for the RC detector and the dipole antenna sensor.

The PDIV test indicated that PDIV occurred at voltages exceeding 9 kV, which serves as a reference for subsequent PD tests. Results from the dipole antenna revealed that negative PDIV appeared before positive PDIV. This observation aligns with the behavior of PD in needle-plate electrodes tested under air insulation. For positive PD, electrons originate from the SF₆ gas, whereas for negative PD, electrons are emitted from the needle. Negative PD occurs first because the energy required to generate an initiating electron on the needle is lower than that required to produce an electron from SF₆ gas. Consequently, the energy and voltage necessary to initiate negative PD are lower than those for positive PD.

Table 7. Negative and positive PDIV on the sensor

| Sensor name | Positive PDIV (kV) | Negative PDIV (kV) |
|----------------|--------------------|--------------------|
| RC detector | 10.3 kV | 10.06 kV |
| Dipole Antenna | 13.3 kV | 10.06 kV |

4.3.2. Waveform measurement

Based on previous PDIV testing, PDIV was observed at voltages exceeding 9 kV. For the waveform measurement, the partial discharge waveform was recorded at voltages above both the negative and positive PDIV values. Therefore, this PD test was conducted at a higher voltage level, specifically at 16 kV. The resulting waveforms from the dipole antenna, as detected by both the RC detector and the dipole antenna sensor, are presented in the Figure 7. The Figure 7 illustrates a dipole antenna, demonstrating that the waveform represents the simultaneous occurrence of RC waves and antenna waves. When PD occurs, the dipole antenna generates a greater number of waves compared to the RC detector.

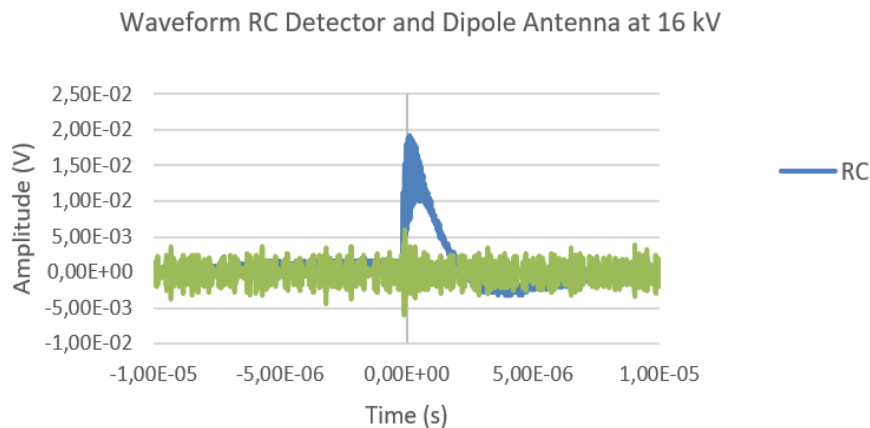


Figure 7. Waveform RC detector and dipole antenna at 16 kV

5. CONCLUSION

Dipole antennas designed for the UHF frequency range (300 MHz to 3 GHz) demonstrate that variations in design parameters have a significant impact on antenna performance. In previous research, A 66×15 mm dipole antenna yielded a bandwidth of 336 MHz, a return loss of -22.4 dB, and a resonance frequency of 1.3 GHz. Subsequently, after adjusting the length and width of the dipole antenna, the best results were obtained with a size of 35×40 mm. Modifying the antenna length to 35×40 mm results in a maximum bandwidth of 989 MHz and a return loss of -28.47 dB at a resonant frequency of 1.4 GHz. These findings indicate that the designed dipole antenna effectively detects partial discharge in GIS at a voltage level of 16 kV.




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