Vol. 35, No. 2, August 2024, pp. 704~710

ISSN: 2502-4752, DOI: 10.11591/ijeecs.v35.i2.pp704-710

Lifetime (B_x) improvement of PV inverter using Si-SiC H-IGBT/Diode: a reliability approach

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Article Info

Article history:

Received Feb 6, 2024 Revised Mar 3, 2024 Accepted Apr 7, 2024

Keywords:

H-IGBT/diode Lifetime (Bx) PV inverter Reliability Silicon Silicon carbide

ABSTRACT

Technological advancements have made it possible to harness the power of renewable energy sources. The efficiency of power electronic devices has increased to almost 98%. In order to reduce the risks of failure and maintain the operation of photovoltaic (PV)-based energy converters, reliable devices are needed. Due to the increasing number of wide-bandgap silicon in electronic converters, the need for more efficient and reliable devices has become more prevalent. However, the cost of these devices is a major issue. Hence, in this work extensive analysis of hybrid silicon (Si)-IGBT and silicon carbide (SiC) antiparallel Diode (H-IGBT/Diode) based PV inverter is proposed to improve the lifetime (Bx). A reliability oriented lifetime assessment is performed on a test case of single stage three kilowatt photovoltaic inverter with 600 V/30 A hybrid switch. Long term mission profile for one year is considered for evaluation at B. V. Raju Institute of Technology (BVRIT), Telangana, India. Finally, B10 lifetime is calculated, comparison analysis is presented between conventional Si-IGBT and proposed Si-SiC H-IGBT/Diode. The results of the study revealed that the H-IGBT exhibited a significant increase in PV inverter reliability.

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704

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1. INTRODUCTION

Due to the increasing number of RES, the need for power electronic devices has also increased. In most systems, the cost of power electronic converters is around 59%. Thermal stress is a common issue that affects power semiconductors. It can cause various issues, such as solder-die fatigue and lift-off [1]. Due to the high cost of maintaining power electronic devices, it is important that they are modified to reduce their risk of failure. To provide high reliability, power electronic devices are required for photovoltaic (PV) energy conversion systems. Due to the limitations of current-generation power electronic devices, such as those based on Si, conventional switches are not able to meet the needs of the market [2], [3]. A type of power electronic switch that is based on silicon carbide (SiC) technology offers a wide bandgap, which makes it more effective than its conventional counterparts. The other advantages of this type of device include its high switching speed and low switching losses. The rising cost of SiC components is one of the biggest concerns for the PV inverter market. Since it is not feasible to replace every device in the system with this type of technology, hybrid solutions have been proposed [4].

The mathematical model for the turn-off process of a hybrid switch is established by performing a double pulse test. The factors that influence the turn-off velocity and working conditions of the switch are analyzed in [5]. The characteristics of SiC and IGBTs, which are commonly used in SSC, are studied in [6].

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In addition, the junction temperature and load current laws are analyzed. Yin *et al.* [7] developed a hybrid FBSM that features a SiC IGBT and a SiC MOSFET. In addition, a control scheme is proposed that will optimize the current path of the FBSM. It will also concentrate the high-frequency switching on the SiC module and improve its compatibility with the MMC modulation scheme. Woldegiorgis *et al.* [8] presented an extensive evaluation and comparison of different gate control techniques, as well as various packaging approaches. It also offers a general guideline for choosing the right approach for specific applications. The study highlights the advantages of utilizing Si/SiC materials and provides a comprehensive understanding of their switch design characteristics.

The dual-inverter configuration, which combines the SiC-MOSFET and Si-IGBT technologies, can be used in cars with premium class driving characteristics and lower power consumption are proposed in [9]. Efficient results and logical arguments support the concept are presented in this research. Bei and Le [10] proposed an optimized switching mode for the hybrid parallel devices based on the characteristics of the SiC IGBT/MOSFET devices. Walter and Bakran [11] aims to improve the overall power loss of a traction inverter that is operating at a DC-Link voltage of 400 V. It utilizes a 650V Freewheeling Diode and a 650 V Si-MOSFET dual in parallel. In addition, it presents a method to decouple the IGBT/SIGBT and SiC-MOSFET halves by using a small inductance. The relationship between the gate turnoff time and the power loss of the Si/SiC hybrid switch has been studied in [12]. It has been revealed that the optimal delay time is between 1 and 2 seconds, which can be used for the switch's minimum turn-off loss. Increasing the working current of the hybrid switch will also decrease the delay time. Cheng et al. [13] developed a 30 kW 12 V iHPM incorporating 30 kHz SiC/Si integrated technology. It will be used in industrial drive applications such as motors for variable frequency drives. Diao et al. [14] proposed a 5-level hybrid ANPC converter with an inner-interleaved design. It features improved output quality and an easier filtering design. The converter is composed of various low-frequency switching cells and high-frequency MOSFETs. The cost-effective and high-efficiency of this converter are mainly attributed to its low-noise characteristics. Diao et al. [15] presented a megawatt-sized MV hybrid electric power conversion prototype. Related works are presented in [16]–[23]. It aims to evaluate the feasibility of this technology in the next-generation aircraft system. In addition to being able to provide electric propulsion, this prototype can also be used onboard a 3-kilowatt DC bus.

In this paper hybrid silicon (Si)-IGBT and SiC antiparallel diode (H-IGBT/Diode) based PV Inverter is proposed to improve the lifetime (B_x). A reliability oriented lifetime assessment is performed on a test case of single stage three kilowatt photovoltaic inverter with 600 V/30 A hybrid switch. Long term mission profile for one year is considered for evaluation at BVRIT, Telangana, India. Junction temperature (T_J) is calculated for corresponding mission profile. T_J variations are analyzed using the rainflow counting (C_R) algorithm. Monte Carlo simulation (S_{MC}) approach is utilized and generated 20,000 samples with five percentage variation. Finally, B_{10} lifetime is calculated at component level (L_C) and system level (L_S). Comparison analysis is presented between conventional Si-IGBT and proposed Si-SiC H-IGBT/Diode. The results of the study revealed that the H-IGBT exhibited a significant increase in PV inverter reliability.

2. PROPOSED Si-SiC H-IGBT/DIODE SWITCH FOR PV INVERTER

The use of silicon carbide in power electronic devices has revolutionized the way we think about power electronics. Its exceptional thermal conductivity and wide bandgap enable the development of innovative switches that are capable of operating at high temperatures and voltages. Switching devices for high-voltage applications, such as power converters and electric cars, are commonly made using silicon carbide. Its various advantages, such as its compact size and better efficiency, make it a suitable choice for numerous industries. Due to the significant cost and complexity of silicon carbide switches, several companies, such as Infineon, STMicroelectronics, and Cree, have been leading the way in producing these components. These companies contributions have helped push the envelope of power electronics [24]–[26]. The Comparison of Si and SiC are presented in Table 1. Still SiC based switches are not economical in this paper Si-SiC H-IGBT/Diode based photovoltaic inverter is proposed as shown in Figure 1. The proposed system is implemented in PLECS environment. The Si-IGBT thermal model is based on the Infineon manufacturer. On the other hand, the SiC-Diode model is from the wolfspeed manufacturer.

Table 1. Comparison

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Material	Breakdown voltage (10 ⁶ V/cm)	Thermal conductivity (λ)	Bang gap (eV)	
Silicon (Si)	0.3	1.5	1.1	
Silicon Carbide (SiC)	2.4	4.5	3.3	

706 □ ISSN: 2502-4752

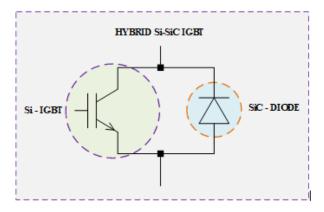


Figure 1. Proposed H-IGBT/Diode

3. RELIABILITY ORIENTED LIFETIME (Bx) ASSESSMENT METHOD

The reliability-oriented lifetime (B_x) assessment method follows several steps. To consider environmental conditions, long term mission profile i.e., Solar Irradiance (I_{RR}) and Ambient Temperature (T_A) for one year is considered for evaluation at B V Raju Institute of Technology (BVRIT), Telangana, India in step 1. T_J is calculated using Foster ETM in the step 2. T_J variations are analyzed using the rainflow counting (C_R) algorithm in step 3. Bayerer's lifetime (L_F) equation is used to calculate the lifetime as shown in (1):

$$L_{F} = \frac{\frac{1}{\sum \frac{N_{i}}{K(\Delta T_{j})^{\beta_{1}} e^{\left(T_{j}+273K\right)}} \int_{ton}^{R_{3}} dA_{i} V^{\beta_{5}} dA_{6}}}$$
(1)

 S_{MC} approach is utilized and generated 20,000 samples with five percentage variation in step 4. The distribution of the generated 20,000 samples were carried out through the Weibull process and the R(t) is calculated as follows:

$$R(t) = e^{-\left(\frac{t}{\infty}\right)^{\gamma}} \tag{2}$$

where \propto = scale parameter.

 γ = shape parameter.

$$R_{total}(t) = \prod_{i=1}^{n} R_i(t)$$
(3)

Where $R_i(t)$ individual component reliability.

Finally, reliability-oriented lifetime (B_x) assessment is evaluated in step 5. The detailed flowchart is presented in Figure 2.

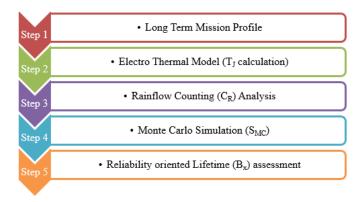


Figure 2. Flowchart

4. TEST CASE

In this work extensive analysis of hybrid silicon (Si)-IGBT and SiC antiparallel Diode (H-IGBT/Diode) based PV Inverter is proposed to improve the lifetime (B_x). A reliability oriented lifetime assessment is performed on single stage three kilowatt photovoltaic inverter with 600 V/30 A hybrid switch as shown in Figure 3. The specifications of the system are tabulated in Table 2.

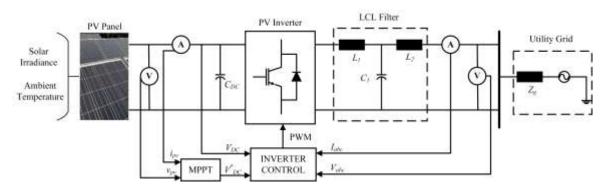


Figure 3. Proposed test case system

Table 2. Parameters

Name	Specification	
Model and Make of PV Panel	BP solar (365)	
Rating of Inverter	Three kilowatt	
RMS Voltage at Grid	230 V	
Frequency at Grid	50 Hz	

5. RESULTS AND DISCUSSION

In this work reliability oriented lifetime (B_x) assessment. Is evaluated for the proposed Si-SiC H-IGBT/Diode and compared with conventional Si-IGBT. The assessment is carried as per the Figure 2.

5.1. Long term mission profile at BVRIT

To consider environmental variations, long term mission profile i.e., solar irradiance (I_{RR}) and ambient temperature (T_A) for one year is considered for evaluation at B V Raju Institute of Technology (BVRIT), Telangana, India from September 2020 to August 2021. The yearly mission profile is presented in Figure 4. Where solar irradiance (I_{RR}) is presented in Figure 4(a) and ambient temperature (T_A) is presented in Figure 4(b).

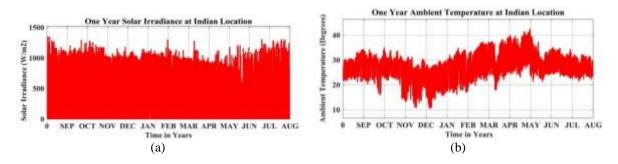


Figure 4. Long term mission profile (a) solar irradiance and (b) ambient temperature

5.2. Electro thermal model

Long term yearly mission profile i.e., I_{RR} and T_A are translated to T_J using the foster electro thermal model. The translated T_A for conventional Si-IGBT and proposed Si-SiC H-IGBT/Diode corresponding to the long term mission is presented in Figure 5. The average T_J for the convention Si-IGBT is 55.66 °C, for proposed H-IGBT/Diode is 53.9 °C. The average T_J is decreased using the proposed H-IGBT/Diode as shown in Figure 6.

708 □ ISSN: 2502-4752

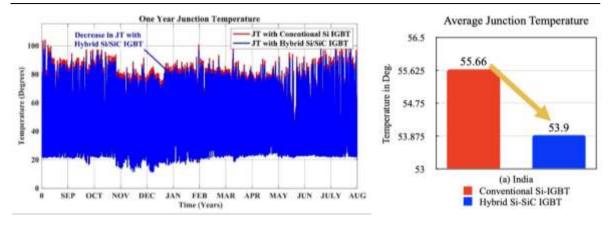


Figure 5. Translated T_J for long term mission profile

Figure 6. Average T_J

5.3. Rainflow counting (C_R) analysis

To analyze the variations of the translated T_J is analyzed using rainflow counting (C_R) . C_R parameters No.of Cycles N_i , mean junction temperature T_{jm} , cycle amplitude ΔT are obtained for both conventional Si-IGBT as shown in Figure 7. Proposed H-IGBT/Diode as shown in Figure 8 respectively.

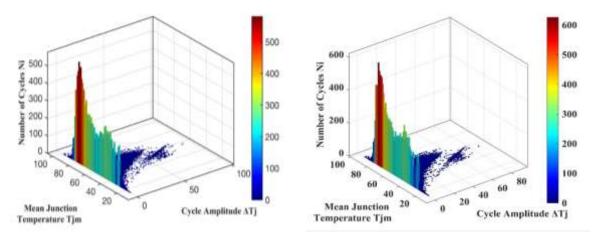


Figure 7. C_R analysis for conventional Si-IGBT

Figure 8. C_R analysis for proposed H-IGBT/Diode

5.4. Monte Carlo simulation (S_{MC})

SMC approach is utilized and generated 20,000 samples with five percentage variation and L_F is calculated at all the samples using (1) and fitted in the Weibull distributions for both conventional Si-IGBT as shown in Figures 9. Proposed H-IGBT/Diode as shown in Figure 10 respectively.

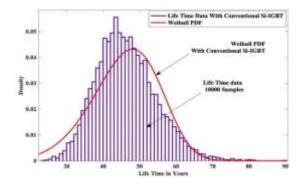


Figure 9. S_{MC} for conventional Si-IGBT

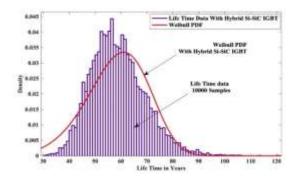


Figure 10. S_{MC} for proposed H-IGBT/Diode

5.5. Reliability oriented lifetime (Bx) assessment

Reliability oriented lifetime (B_{10}) assessment is evaluated for conventional Si-IGBT and proposed H-IGBT/Diode for both L_C and L_S as shown in Figures 11 and 12 respectively. From the above results lifetime (B_x) is improved at both L_C and L_S with the proposed Si-SiC H-IGBT/Diode. At L_C Lifetime (B_x) is improved from 34 years to 42 years. At L_S Lifetime (B_x) is improved from 24 years to 31 years.

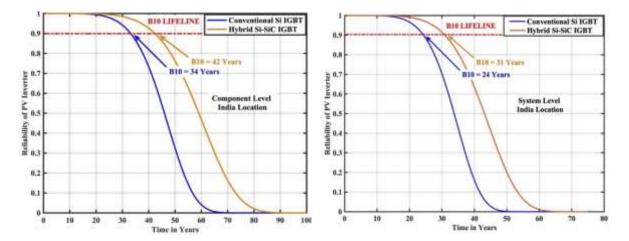


Figure 11. Lifetime (B_x) assessment at L_C

Figure 12. Lifetime (B_x) assessment at L_S

6. CONCLUSION

In this paper hybrid silicon (Si)-IGBT and SiC antiparallel diode (H-IGBT/Diode) based PV inverter is proposed to improve the lifetime (B_x). A reliability oriented lifetime assessment is performed on single stage three kilowatt inverter with 600 V/30 A hybrid switch. Long term mission profile for one year is considered for evaluation at B V Raju Institute of Technology (BVRIT), Telangana, India. Junction temperature (T_J) is calculated for corresponding mission profile. T_J variations are analyzed using the rainflow counting (C_R) algorithm. SMC approach is utilized and generated 20,000 samples with five percentage variation. Finally, B_{10} lifetime is calculated at component level (L_C) and system level (L_S). Comparison analysis is presented between conventional Si-IGBT and proposed Si-SiC H-IGBT/Diode. The results of the study revealed that the lifetime (B_x) is improved at both L_C and L_S with the proposed Si-SiC H-IGBT/Diode. At L_C Lifetime (B_x) is significantly improved from 34 years to 42 years. At L_S Lifetime (B_x) is improved from 24 years to 31 years. In the future the work can be extended by designing the SiC based IGBT.

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