Analysis study of quality factor and bit error rate at wavelength change

Fadhela Thaeer Mahmood¹, Alaa H. Ali¹, Alaa H. Ali Haeder²

¹Department of Electrical Engineering, University of Technology- Iraq, Baghdad, Iraq ²Laser and Optoelectronics Research Center Directorate of Ministry of Science and Technology Baghdad, Baghdad, Iraq

Article Info	ABSTRACT
Article history:	Gigabit-per-second data speeds can be achieved via free space optics (FSO)
Received Feb 28, 2022 Revised Apr 22, 2022 Accepted May 30, 2022	lines, which needless system complexity. On the other hand, the link's availability across a wide range of atmospheric circumstances is a major worry. As a result of the increased signal attenuation caused by the linkages being weather-dependent, their efficiency decreases. Up to 70 dB/km of attenuation can be caused by bad weather on a 500-meter free space optics
Keywords:	link. In this work, transmission windows of 1310 nm, 850 nm, and 1550 nm are analyzed and compared using the free space optics link. by using the
Analyzers-for-attenuation Bit error rate Free space optic Optical transmission windows	Simulation program opti system such as the quality factor, the minimal bit error rate (BER), and the eye diagram is taken into account. Analyzer findings are compared to establish the optimal wavelength for a transmitter under poor weather conditions.
Program optisystem 2015	This is an open access article under the <u>CC BY-SA</u> license.
Program origin 2021	BY SA
Corresponding Author:	
Fadhela Thaeer Mahmood Department of Electrical Engineeri	ng, University of Technology-Iraq

1. INTRODUCTION

Email: eee.20.47@grad.uotechnology.edu.iq

Baghdad, Iraq

An alternative to optical fiber or random forest (RF) systems, free space optics (FSO) uses light propagation in the free space to transport data between two sites. In situations where optical fibers are not an option, Figure 1 shows communications via optical wireless technology, divided into three stages: the first is the transmission, the second is the channel, and the third and final is the receiving stage. FSO systems can be utilized for a variety of purposes, including high-capacity internet access for the last mile and temporary high bandwidth data links. However, the weather can have an impact on FSO communication [1], [2]. FSO offers an unlicensed spectrum for local area networks, easy implementation, no electromagnetic signal interference, and a very fast data transfer rate, This method uses the visible and infrared wavelengths of the optical wave as a means of transmitting the information [3], [4]. Transmissions of light undergo several distortions due to atmospheric turbulence. The centroid of the transmitted beam is shifted by turbulent cells larger than the beam because of the beam's wandering distortion. By widening the beam radius, the beam spreading effect reduces the average intensity at the receiver [5]. Its extreme sensitivity to attenuation in adverse weather and turbulent air conditions makes it vulnerable to these significant free space optic advantages [6]. Fog, rain, snow, and haze all cause light beam loss due to absorption caused by molecule diffusion and scattering, turbulence, scattering, absorption, and attenuation are the basic mechanisms of signal attenuation [7], [8]. With the distortion that occurs in the atmosphere when it rains, electromagnetic waves cannot travel as far as they normally [9]. To start up communication using free space optic technology, it is necessary to maintain an apparent line of sight (LOS) between the transmitter and receiver. Attenuation produced by air conditions reduces the wireless channel's range and capacity [10]. Therefore, limiting the places and periods where the

free space optic link can be used will limit its potential [4] free space optic technology relies on careful weather analysis and the use of different optical windows to limit the effects of rising signal attenuation for its bandwidth to be maximized [11].

The averaged field distributions along. the cavity length was used to construct new analytical models for semiconductor laser amplifiers. The electron concentration may be calculated using the charge conservation equation and this density. An effective spontaneous emission factor was used to quantify the total amplified spontaneous emission over wavelength without taking into consideration the link between gain and spontaneous emission and photon energy. Therefore, the goal of this contribution is to break from this basic assumption and incorporate actual models for gain and spontaneous emission as functions of photon energy and carrier concentrations. Optoelectronic amplifiers' maximum gains can be significantly increased by using anti-reflective coatings. As a result of the higher drive currents required by the amplified spontaneous emission, there is a practical upper limit to the amplifier gains that can be achieved by amplifying the device's maximum practical gain [12]. The three above-mentioned wavelengths were picked from the vast spectrum of spectral wavelengths due to the transmission qualities of available light sources. An information signal flowing through space has a substantially lower attenuation at these frequencies. Attenuation is a result of both absorption and scattering, which affects the quality of the signal. Therefore, these three infrared light wavelengths are chosen above others [13]. When wavelength division multiplexing (WDM) is used, WDM can boost system capacity because it sends many bit streams simultaneously [14].



Figure 1. Communication via optical-wireless technology

2. SYSTEM DESCRIPTION

Figure 2 depicts the free space optic link, which includes the transmitter, atmospheric channel, and receiver. Electrical information streams are modulated into optical signals using a transmitter in the free space optic link (Figure 2) On its way through space, it is caught and turned into an electrical signal by the receiver. The transmitting module consists of a pulse generator, modulator, and transmitter. Information is transmitted using an electrical pulse generator in the link. After that, the signal is broadcast into the atmosphere by the transmitter. It is possible to transfer high-bandwidth digital data without the need for fiber optics using free-space optics (FSO). During the development of an FSO channel, the parameters describe the impacts of atmospheric turbulence and change scatter, absorb, and attenuate signals in the atmosphere. The most critical difficulty with a non-stationary link is the optical beam aiming inaccuracy (or "misalignment") between the transmitter and receiver [8], [15]-[17]. Figure 2 depicts the FSO link block diagram. Figure 2 depicts the FSO link block diagram.

The receiver, which incorporates an amplifier, a photodetector, a filter, and a BER analyzer, accurately decodes the information stream. The link's amplifier boosts the receiving signal's power. The photodetector converts optical signals into electrical signals before transferring them to the filter. The filter's primary function is to reduce external noise while allowing the intended wavelength of the signal to pass through it. Analyze the signal with the bit error rate (BER) analyzer. The BER measures the proportion of wrongly recognized bits received during transmission [18].



Figure 2. Depicts the FSO link block diagram

3. MATHEMATICAL MODEL DESCRIPTION

Many weather conditions can affect free space optic in the troposphere, which is where the transceivers are located in a terrestrial free space optic system. In states with poor visibility, such as rain, snow, fog, and clouds, communication is difficult. An empirical model can be used to estimate the attenuation effects of snow, rain, and fog [19], [20].

$$\alpha_{\rm fog}(\lambda) = \frac{3.912}{V} \left(\frac{\lambda}{55*10^4}\right)^{-q} \tag{1}$$

Where: $\alpha fog(\lambda)$: total extinction coefficient: transmission wavelength in μm , V: visibility range in km, Q: scattering size distribution coefficient to droplet size distribution.

Approximations of the q parameter to Kim and Kruse's model for fog attenuation in clear or only foggy weather can be made [21], [22].

$$q = \begin{cases} 1.6 \ (V \ge 50 \ \text{km}) \\ 1.3 \ (6 \ \text{km} \le V \le 50 \ \text{km}) \\ 0 \ (V \le 0.5 \ \text{km}) \end{cases}$$
(2)

$$q = \begin{cases} 1.6 \text{ if } V > 50 \text{ km}, \\ 1.3 \text{ if } 6\text{km} < 50 \text{ km}, \\ 0.585 V^{\frac{1}{3}} \text{ if } V < 6 \text{ km} \end{cases}$$
(3)

Absorption and scattering are two of the most common ways that optical signals lose power in open space. Water vapor, which is affected by carbon dioxide, humidity, and altitude, is the most common cause of absorption. Another mechanism of optical power loss is scattering, which results in a decrease in optical beam intensity over distance. Using (4), it is possible to calculate the scattering of an optical beam [23], [24].

$$\alpha_{\text{scat}}(\lambda) = \frac{17}{V} \left(\frac{550}{\lambda}\right)^{0.195V}, \text{ db/km}$$
(4)

 $\{\lambda\}$: is a transmission wavelength (in micrometers), and V is the visibility range (in Km). Atmospheric conditions affect the total attenuation of wireless signals.

$$\alpha = \alpha_{\text{fog}} (\lambda) + \alpha_{\text{snow}} + \alpha_{\text{rain}} + \alpha_{\text{scat}} (\lambda), dB/km$$
 (5)

Rain and fog can degrade the optical communication signal as it travels through the atmosphere. Fog is the primary source of attenuation for optical wireless links. We can't ignore the attenuation effect of rain in areas where fog is more common. With increasing droplet size, the refraction and reflection processes increase. The rain droplet's attenuation for a wireless optical link can be provided by [25], [26].

$$\propto_{rain} = 1.076 \, \mathrm{R}^{0.67} \, \mathrm{dB/Km}$$
 (6)

The mm/hour is the rate of rainfall (R). In terms of decibels per kilometer, snow's specific attenuation is given by [27] as (7).

$$\alpha_{\rm snow} = a \, {\rm S}^{\rm b} \, \frac{d{\rm B}}{{\rm K}m} \tag{7}$$

In computing, a "bit error rate" (BER) is a measure of how likely it is that an incorrectly identified bit will occur. The inverse relationship between BER and signal to noise ratio (SNR) may be seen in the graph below. The noise in large avalanche photodiodes (APD) receivers is thermally restricted, which is independent of the signal current. The following expression can be used to calculate BER to SNR [28].

BER
$$\approx \left(\frac{2}{\pi.SNR}\right) \cdot \exp\left(\frac{-SNR}{8}\right)$$
 (8)

4. ANALYZING SYSTEM MODELS BASED ON BER ANALYZER OUTPUT

We measure quality factor and bit error rate by bit error rate analyzer (BERA). Using three wavelengths (850 nm, 1310 nm, and 1550 nm). With each wavelength we use atmospheric attenuation (5, 20, 40, 70) dB/km for a distance of 500 m.

4.1. Distance 500 m with wavelength 850 nm

When connecting the circuit by using a distance of 500 m and a wavelength of 850 nm to find out the effect of the signal carried by the wavelength on the attenuation. We took the attenuation in the limits (5, 20, 40, 70) dB/km as shown in Figures 3 to 6). The results are in Table 1.



Figure 3. Analyzer output at 5 dB/km attenuation



Figure 5. Analyzer output at 40 dB/km attenuation

Figure 4. Analyzer output at 20 dB/km attenuation



Figure 6. Analyzer output at 70 dB/km attenuation

Table 1. Wavelength 850 nm, distances 500 m				
Attenuation dB/km	Quality factor	Bit Error Rate (BER)		
5	3416.91	0		
20	1430.27	0		
40	653.625	0		
70	98.1382	0		

4.2. Distance 500 m with wavelength 1310 nm

When connecting the circuit by using a distance of 500 m and a wavelength of 1,310 nm to find out the effect of the signal carried by the wavelength on the attenuation. We took the attenuation in the limits of (5, 20, 40, 70) dB/km as shown in Figures 7 to 10). The results are in Table 2.



Figure 7. Analyzer output at 5 dB/km attenuation

Figure 8. Analyzer output at20 dB/km attenuation



Figure 9. Analyzer output, 40 dB/km attenuation



Table 2. Wavelength 1310 nm, distances 500 m				
Attenuation dB/km	Quality factor	Bit Error Rate (BER)		
5	4011.92	0		
20	1613.36	0		
40	638.946	0		
70	89.5579	0		

4.3. Distance 500 m with wavelength 1550 nm

When connecting the circuit by using a distance of 500 m and a wavelength of 1550 nm to find out the effect of the signal carried by the wavelength on the attenuation. We took the attenuation in the limits of (5, 20, 40, 70) dB/km as shown in the Figures 11 to 14. The results are in Table 3.



Figure 11. Analyzer output, 5 dB/km attenuation

Figure 12. Analyzer output, 20 dB/km attenuation



Figure 13. Analyzer output, 40 dB/km attenuation

Figure 14. Analyzer output, 70 dB/km attenuation

Table 3. Wavelength 1550 nm, distances 500 m				
Attenuation dB/km	Quality factor Bit Error Rate (BE			
5	1502.88	0		
20	605.046	0		
40	168.604	0		
70	23.5829	$2.09208 e^{-123}$		

Comparison between the results of Shaina and Gupta [13] and the proposed work, of the extent to which wavelengths are affected by attenuation on the quality factor and error bit adjustment, for a distance of 500 m as shown in Table 4. Using the origin program, to draw the relationship between Q-factor and attenuation, was plotted using three windows at 850 nm, 1310 nm, and 1550 nm for a distance of 500 meters, in the Figure 15 shown here the lower the distance the higher the quality factor and vice versa was found to be the case.

Tabel 4 A distance of 500 m

Tabel 4. A distance of 500 m					
Attended in a D land	5 dB/km 20 dB/km 40 dB/km	70 dB/km			
Auenuauon ud/km	Q-factor BER Q-factor BER Q-factor BER	Q-factor BER			
Wavelength 850 nm, 500 m Shaina and Gupta [13]	2860.26 0 1112.54 0 195.015 0	8.1304 0			
(Proposed Work)	3416.91 0 1430.27 0 653.625 0	98.1382 0			
Wavelength 1310 nm,500 m Shaina and Gupta [13]	3000.90 0 1156.01 0 192.498 0	7.95898 8.66465e ⁻⁰¹⁶			
(Proposed Work)	4011.92 0 1613.36 0 638.946 0	89.5579 0			
Wavelength 1550 nm,500 m Shaina and Gupta [13]	255.869 0 108.37 0 30.27 9.17421e ⁻²⁰²	2.95239 0.00153508			
(Proposed Work)	1502.88 0 605.046 0 168.604 0	23.5829 2.09208e ⁻¹²³			
Quality factor (Q-factor) Bit error rate (BER)					

Quality factor (Q-factor), Bit error rate (BER)



Figure 15. Relation between Q-factor and attenuation at (850, 1310, 1550) nm to distance 500 m

5. CONCLUSION

The 850 nm, 1310 nm, and 1550 nm optical transmission windows were utilized to evaluate the free space optic communication link in varied air circumstances over distances ranging from 500 meters. Under low attenuation conditions, propagation distance and bit error rate are observed to be greatest at 1550 nm wavelength. As a result, 1550 nm should be the wavelength of choice for low attenuation. It exhibits lower bit error rates under high attenuation situations because of its big Q factor and eye height, according to simulation data. Optical transmission at 1310 nm gives better outcomes and is safer for users than 850 nm transmission at 850 nm spectral lines 1310 nm attenuation values are the best for transmitting. Attenuation and quality were shown to increase in direct proportion to the distance traveled.

REFERENCES

- A. K. B. Rahman *et al.*, "Impact of rain weather over free space optic communication transmission," *Indonesian Journal of Electrical Engineering and Computer Science*, vol. 14, no. 1, pp. 303–310, Apr. 2019, doi: 10.11591/ijeecs.v14.i1.pp303-310.
- [2] D. Saha, J. Roy, K. F. Fiaboe, and P. Kumar, "Design and analysis of FSO (free space optics) link at high bit rate," in Proceedings of the 3rd International Conference on Inventive Systems and Control, ICISC 2019, Jan. 2019, pp. 62–66, doi: 10.1109/ICISC44355.2019.9036358.
- [3] M. A. Khalighi and M. Uysal, "Survey on free space optical communication: A communication theory perspective," *IEEE Communications Surveys and Tutorials*, vol. 16, no. 4, pp. 2231–2258, 2014, doi: 10.1109/COMST.2014.2329501.
- [4] A. Almukhtar, A. Abass, and M. Ali, "Effect of fiber-telescope coupling losses on wideband wavelength division multiplexing in free space optical communications," *Engineering and Technology Journal*, vol. 40, no. 2, pp. 350–357, Feb. 2022, doi: 10.30684/etj.v40i2.2194.
- [5] J. Kalati and S. Kadhim, "Design analysis of a compensation technique in FSO communication system to mitigate atmospheric turbulence effect," *Engineering and Technology Journal*, vol. 37, no. 3B, pp. 82–85, Oct. 2019, doi: 10.30684/etj.37.3b.3.
- [6] A. Vavoulas, H. G. Sandalidis, and D. Varoutas, "Weather effects on FSO network connectivity," *Journal of Optical Communications and Networking*, vol. 4, no. 10, pp. 734–740, Oct. 2012, doi: 10.1364/JOCN.4.000734.
- [7] M. Ijaz, Z. Ghassemlooy, J. Perez, V. Brazda, and O. Fiser, "Enhancing the atmospheric visibility and fog attenuation using a controlled FSO channel," *IEEE Photonics Technology Letters*, vol. 25, no. 13, pp. 1262–1265, Jul. 2013, doi: 10.1109/LPT.2013.2264046.
- [8] A. A. B. Anis, C. B. M. B. Rashidi, and S. A. Aljunid, "Analysis using multiple free space optic channel with amplification to mitigate haze attenuation," *Indonesian Journal of Electrical Engineering and Computer Science*, vol. 14, no. 2, pp. 546–554, May 2019, doi: 10.11591/ijeecs.v14.i2.pp546-554.
- [9] M. A. Samad, M. R. Ahmed, and S. Z. Rashid, "An overview of rain attenuation research in Bangladesh," *Indonesian Journal of Electrical Engineering and Computer Science*, vol. 23, no. 2, pp. 902–909, Aug. 2021, doi: 10.11591/ijeecs.v23.i2.pp902-909.
- [10] F. Hossain and Z. Afroze, "Eliminating the effect of fog attenuation on FSO link by multiple TX/RX system with travelling wave semiconductor optical amplifier," in *Proceedings of 2013 2nd International Conference on Advances in Electrical Engineering, ICAEE 2013*, pp. 267–272, doi: 10.1109/ICAEE.2013.6750345.
- [11] S. Saini and A. Gupta, "Investigation to find optimal modulation format for low power inter-satellite optical wireless communication (LP-IsOWC)," in *IFIP International Conference on Wireless and Optical Communications Networks, WOCN*, Sep. 2014, pp. 1–4, doi: 10.1109/WOCN.2014.6923094.
- [12] I. D. Henning, M. J. Adams, and J. V. Collins, "Performance Predictions from a new optical amplifier model," *IEEE Journal of Quantum Electronics*, vol. 21, no. 6, pp. 609–613, Jun. 1985, doi: 10.1109/JQE.1985.1072709.
- [13] Shaina and A. Gupta, "Comparative analysis of free space optical communication system for various optical transmission windows under adverse weather conditions," *Procedia Computer Science*, vol. 89, pp. 99–106, 2016, doi: 10.1016/j.procs.2016.06.014.
- [14] A. Y. Fattah and A. R. Farhan, "Spectral Efficiency improvement of the optical communication systems," Iraqi Journal of Computers, Communication, Control & Systems Engineering (IJCCCE), vol. 14, no. 1, pp. 44–57, 2014.
- [15] A. K. Majumdar and J. C. Ricklin, Free-Space Laser Communications. New York, NY: Springer New York, 2008, doi: 10.1007/978-0-387-28677-8.
- [16] A. K. B. Rahman et al., "Spectral coding performance under free space optical medium," Indonesian Journal of Electrical Engineering and Computer Science, vol. 14, no. 1, pp. 290–294, Apr. 2019, doi: 10.11591/ijeecs.v14.i1.pp290-294.

- [17] A. J. Mahdi, W. J. Mazher, and O. N. Ucan, "Impact of pointing error on SISO/MISO drones swarm-based free space optical system in weak turbulence regime," *Indonesian Journal of Electrical Engineering and Computer Science*, vol. 23, no. 2, pp. 918– 926, Aug. 2021, doi: 10.11591/ijeecs.v23.i2.pp918-926.
- [18] A. El-Naser A. Mohamed, "Integrated service quality enhancement of wireless optical communication systems for long haul transmission distances," *Journal of Engineering and Computer Innovations*, vol. 2, no. 9, Dec. 2011, doi: 10.5897/jeci11.050.
- [19] R. Bajwa and P. Verma, "Effect of different atmospheric conditions on the performance of the FSO system at 1550 nm," in 2018 5th International Conference on Signal Processing and Integrated Networks, SPIN 2018, Feb. 2018, pp. 390–395, doi: 10.1109/SPIN.2018.8474154.
- [20] M. Sultana, A. Barua, J. Akhtar, and M. I. Reja, "Performance investigation of OFDM-FSO system under diverse weather conditions of Bangladesh," *International Journal of Electrical and Computer Engineering*, vol. 8, no. 5, pp. 3722–3731, Oct. 2018, doi: 10.11591/ijece.v8i5.pp3722-3731.
- [21] S. Singh and G. Soni, "Pointing error evaluation in FSO link," in *IET Conference Publications*, 2013, vol. 2013, no. 645 CP, pp. 365–370, doi: 10.1049/cp.2013.2215.
- [22] F. Nadeem, V. Kvicera, M. S. Awan, E. Leitgeb, S. S. Muhammad, and G. Kandus, "Weather effects on hybrid FSO/RF communication link," *IEEE Journal on Selected Areas in Communications*, vol. 27, no. 9, pp. 1687–1697, Dec. 2009, doi: 10.1109/JSAC.2009.091218.
- [23] A. M. Alatwi, A. N. Z. Rashed, A. S. Parvez, B. K. Paul, and K. Ahmed, "Beam divergence and operating wavelength bands effects on free space optics communication channels in local access networks," *Journal of Optical Communications*, pp. 1–9, Aug. 2020, doi: 10.1515/joc-2019-0276.
- [24] M. N. O. Sadiku, S. M. Musa, and S. R. Nelatury, "Free space optical communications: an overview," *European Scientific Journal, ESJ*, vol. 12, no. 9, p. 55, Mar. 2016, doi: 10.19044/esj.2016.v12n9p55.
- [25] S. S. Muhammad, "Characterization of fog attenuation in terrestrial free space optical links," *Optical Engineering*, vol. 46, no. 6, p. 066001, Jun. 2007, doi: 10.1117/1.2749502.
- [26] P. Paliwal, J. Shreemali, P. Chakrabarti, and S. Poddar, "Performance optimization of hybrid RAMAN-EDFA based WDM-FSO under adverse climatic conditions," *Materials Today: Proceedings*, Feb. 2021, doi: 10.1016/j.matpr.2020.12.624.
- [27] O. Networks and B. Mukherjee, "Free space optical communication," in LIA Today, vol. 10, no. 1, 2002, p. 1.
- [28] D. Jain and R. Mehra, "Performance analysis of free space optical communication system for S, C and L band," in 2017 International Conference on Computer, Communications and Electronics, COMPTELIX 2017, Jul. 2017, pp. 183–189, doi: 10.1109/COMPTELIX.2017.8003961.

BIOGRAPHIES OF AUTHORS



Fadhela Thaeer Mahmood D S S D born in Iraq/Baghdad in May 1989, holds a BSc from the Faculty of the Electrical Engineering/Communications Branch/University of Technology in 2012-2013, and currently studying for an MSc degree from the Department of Electrical Engineering/majoring in Electronics and Communications from the same university. She can be contacted at email: eee.20.47@grad.uotechnology.edu.iq.



Alaa H. Ali D XI Se P Was born in Baghdad, Iraq in 1970. He received his B.Sc and M.Sc degrees in 1993 and 2002 respectively from MEC, Iraq. From 2004-to 2007, he joined a Ph.D. study at the Faculty of Laser and Optoelectronic Engineering, University of Technology, Iraq. Since 2012, he has been Assistant Professor of Optoelectronic Eng. He started scientific publishing in 2003, he has more than 20 publications in national and international conferences and journals. His research interests are in optical fiber design, optical fiber communications, wired communications, and optical sensors. He can be contacted at email: alaa.h.ali@uotechnology.edu.iq.



Alaa H. Ali Haeder 💿 🔀 🔄 P was born in Iraq/Baghdad in June 1975, he obtained a BSc of Science degree from the College of the Science/University of Baghdad in 1999 and an MSc degree from the Department of Applied Sciences/University of Technology in 2005, the Ph.D. degree in laser and optoelectronics sciences in 2012 from the Laser Institute for Postgraduate Studies/University of Baghdad, In the year 2000, he began working in the military industries for three years, then joined the Ministry of Science and Technology until now. He has more than 24 published research papers. He can be contacted at email: alaa.spectro@gmail.com.