

Development of a new rain attenuation model for tropical location

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ABSTRACT

This study proposes a new rain attenuation prediction model (RAM) based on the rain cell concept for tropical locations. The new model addresses the research gap in the international telecommunications union (ITU) model. Results obtained show that the proposed RAM predicted the possibility of signal across seven (7) out of thirteen (13) stations monitored. The predicted attenuation values were 18.3427 dB, 18.8106 dB, 18.3921 dB, 13.8062 dB, 20.8803 dB, 9.4519 dB, and 19.6018 dB for Jalingo, Jos, Makurdi, Mubi, Otukpo, Sokoto, and Abuja respectively. However, the RAM predicted outage across six stations with predicted attenuation values of 31.7040 dB, 26.8302 dB, 28.6635 dB, 29.6562 dB, 28.8827 dB, and 30.0614 dB for Akwa-Ibom, Benin, Donga, Port-Harcourt, Owerri, and Abuja respectively. The proposed RAM hence suggests an additional Ku-band spot beam power of at least 331.97 watts for Nigeria's Nigerian communication satellite-1 (NIGCOMSAT-1R) Ku-band transponder to overcome the predicted attenuation across the six stations which recorded signal outage. The results from this study can be used by network engineers for the implementation of fade mitigation techniques (FMTs) such as site diversity and power control to aid telecommunication networks anticipate changes and allocate resources accordingly.

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1. INTRODUCTION

Attenuation due to rain increases significantly especially for frequencies exceeding 10 GHz. Tropical locations such as Nigeria are characterized by high rainfall rates and large raindrop sizes. Successful studies on the impact of rain on earth-space communication links have been carried out over the years. To determine the appropriate fade margins and diversity factors for earth-space communication links, studies on the performance and prediction of attenuation due to rain on earth-space links become necessary. Research campaigns by [1]-[5] over tropical and temperate climate by [6] amongst others provide experimental results for attenuation prediction due to rainfall. As such, more studies are needed in tropical locations such as Nigeria since attenuation prediction due to rain is location-specific.

The international telecommunications union recommendation (ITU-R) recommends a global rain-attenuation prediction model for satellite links but it lacks physical meaning because it is an empirical model while the estimation of the effective path length is dependent on both frequency and elevation angle [1]. The rain attenuation predicted by the ITU-R model varies non-monotonically with percentage of time and rain

rate in low latitudes (between 36 °S and 36 °N) and low elevation angles below 25° [2]. To this end, a new rain attenuation prediction method is proposed based on the effective number of rain cells. The performance of the proposed model is compared with the ITU-R model [7], the Bryant model [4], the Svajatorgor model [8], and the Garcia model [9]. The proposed model is hybrid and takes advantage from both the empirical and physical methods to provide better prediction accuracy when compared with on-site measurements and other existing models. Finally, the anomalous behaviors from other models are improved in the proposed model.

2. RELATED WORK

According to [10], a rain cell is a volume in which convective events occur. There have been some proposed models based on the rain cell concept and physical approaches. The cylindrical cell model [11], [12] was proposed under the assumption that rainfall in the rain cell is uniform. Another prominent model based on weather radar measurements is the EXCELL model [13], [14]. For the horizontal cross-section of the rain cell, the EXCELL model included monoaxial and biaxial models. A better version of the model was recently proposed, and it was based on rain type discrimination. The SC EXCELL model, sometimes known as the modified EXCELL model [14], is a popular name for it. A new model [15] was developed that included both an exponential and a Gaussian component in the rain cell. The exponential component describes the stratiform-like low rain rate outside the cell, while the Gaussian component describes the convective-like high rain rate core. The goal of this study's experimental attempt is to collect data on signal levels and rain rate during signal propagation sessions on satellite-to-earth links. The availability of rain attenuation data improves the precision of rain attenuation estimates and provides a foundation for the development of household rain attenuation models [16]-[20].

The rain attenuation experimental setup includes equipment that monitors both the precipitates and the satellite signal at the same time. The Nigerian environmental and climate observatory programme (NECOP) station, the tropical rainfall measurement mission data (TRMM), the Nigerian meteorological agency (NiMet), and rain gauge experiments are all used to measure precipitation. Empirical and physical methodologies are used in general investigations on rain attenuation. The physical method seeks to replicate the actual physical behavior of the attenuation process from the satellite to the earth station, whereas the empirical method is based on measurements from databases from various climatic zones and stations. Although the empirical method is advocated in [21]-[23], when applied to terrestrial radio communications operating in equatorial and tropical climates, the empirical prediction method produces unsatisfactory results. The prediction model proposed by [24]-[26] has confirmed this claim. In [17], [18] have created some more rain attenuation prediction models for terrestrial and earth-space linkages. These models, on the other hand, are primarily tailored for equatorial and temperate climates [27]-[29]. This research proposes a new rain attenuation prediction model that may be used to estimate wireless radio signal coverage in rainy environments, particularly in tropical areas.

3. RESEARCH METHOD

In this section, the experimental setup for signal downlink from Nigeria's Nigerian communication satellite-1 (NIGCOMSAT-1R) Ku-band transponder is explained. The approach, proposed model, and instrumentation are also discussed in this section.

3.1. Experimental setup for beacon experiment

Two different experimental setups are used to calculate the measured attenuation owing to rain. All atmospheric conditions for composite links were taken into account to allow for link margin and uplink power adjustments to compensate for the beacon satellite receiving antenna's losses [30]-[33]. For this work, the NIGCOMSAT-1R satellite specifications are being used, with an orbital position of 42.5 °E and a downlink frequency of 12.519 GHz for Ku-band with horizontal polarization. Two units of separate satellite receiving antennae were co-located in the same rain cell for the experiment. Two beacon receiving terminals in receive-only mode in the digital video broadcasting (DVB-S2) network running in a time division multiple access (TDMA) scheme with additional receiving antennas made up the independent units. The beacon receiving terminals are set up to only receive satellite downlink data, with one monitoring the signal level in clear skies and the other determining the signal level in wet conditions. This is required to determine attenuation due to rain by subtracting the signal level acquired under clear skies from the value obtained under rainy skies, as stated in (1). The technique should be repeated for various rain events, with the appropriate attenuation values noted.

$$\text{Attenuation (dB)} = \text{RSL}_{\text{clear sky}} - \text{RSL}_{\text{rainy}} \quad (1)$$

where $RSL_{clear\ sky}$ is the received signal level in the clear sky while RSL_{rainy} is the received signal level in rain.

3.2. Approach

The beacon signal is received with horizontal receiving polarization on a 90 cm offset parabolic dish at an elevation angle of 42.5 degrees. The NIGCOMSAT-1R satellite's down-converted Ku-band signal is then transmitted to a digital satellite meter and a signal monitoring device for signal level measurement and logging into a computer unit. The geometric specifications for the receiving antenna are as shown in Figure 1, with an antenna diameter of 0.9 m, a height of 3 m, an antenna gain of 37 dB, and an effective isotropic radiated power (EIRP) of 48 to 55 dBw for a 12.519 GHz link.

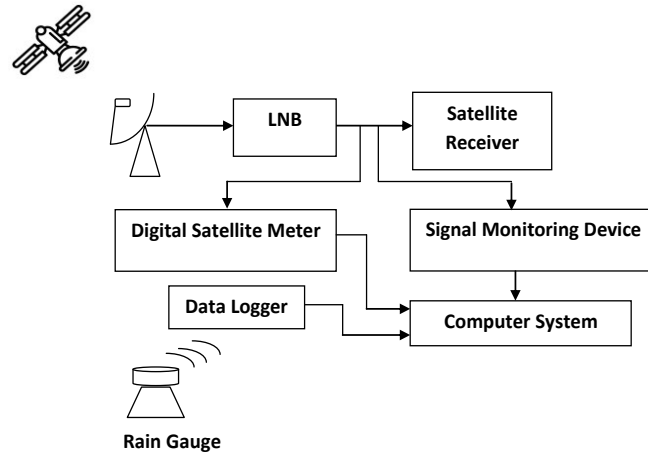


Figure 1. Beacon experiment setup in a tropical location

3.3. Instrumentation

Equipment used to carry out the experiment includes a rain gauge for measuring rainfall rates at different percentages of time, reflector antenna having specific gain, compass, coaxial cable port connector, connecting cable, radiofrequency power meter for measuring power levels, satellite signal tracking device, and timer.

3.4. Proposed model

Daily rainfall rates are obtained and validated using data from the tropical rainfall measurement mission (TRMM) and rain gauge experiments, as well as data from the Nigerian meteorological agency (NiMet) [7]. Recommends using the model presented by [34] to convert rainfall rates to one-minute integration time. There are two types of rain: stratiform ($R < 12$ mm/h) and convective ($R > 12$ mm/h). If a portion of the rain rate is stratiform, the distance is calculated by multiplying the entire time taken by that fraction by an advection velocity of 6 m/s for each rain event. Otherwise, a 10 m/s advection velocity is used for convective cell regions. This technique is performed for each of the threshold values evaluated, and the distances calculated are saved individually. The rain cell number distribution n_2 is predicted by the probability distribution function (PDF) of the distances, whereas the rain cell size distribution n_1 is simply predicted by the cumulative distribution function (CDF) [6]. The effective number of rain cells (N_{eff}) is calculated using the constants n_1 and n_2 . The proposed approach is divided into five steps, as stated in (2)-(9), which are being as:

1) Step one: calculate the effective number of rain cells (N_{eff}) given as:

$$N_{eff} = n_1 + n_2 \tag{2}$$

where: n_1 and n_2 is the rain cell number and rain cell size distribution respectively.

2) Step two: calculate the effective path length for a single rain cell (L_H) as shown in:

$$L_H = \frac{H_R - H_S}{\tan \theta} \text{ [km]} \tag{3}$$

where: H_R = rain height obtained from (26) H_S = station height; θ = elevation angle.

3) Step three: the effective path length (L_{eff}) is now calculated based on the effective number of rain cells in (2) as:

$$L_{\text{eff}} = \frac{L_H N_{\text{eff}}}{\cos \theta} \text{ [km]} \quad (4)$$

where: L_H = effective path length from (3); N_{eff} = effective number of rain cells; θ = elevation angle.

4) Step four: Calculate the attenuation due to rain as:

$$A_{0.01} = \gamma R_{0.01} L_{\text{eff}} \text{ dB} \quad (5)$$

where: L_{eff} is the effective path length given from (4) and $\gamma R_{0.01}$ is the specific attenuation for 99.99% availability obtained from the procedure described in [7] given as:

$$\gamma R_{0.01} = k R_{0.01}^{\alpha} \quad (6)$$

where: k and α are regression constants obtained from [7] and depend on antenna polarization. $R_{0.01}$ is the rainfall rate for 0.01% of time obtained from [34] as shown in:

$$R_{0.01} \text{ (mm/h)} = \alpha M^{\beta} \quad (7)$$

where: M denotes the mean annual accumulation of rain for a given location; α and $\beta = 12.2903$ and 0.2973 respectively.

5) Step five: calculate attenuation for other percentages of time p as shown in:

$$A_p \text{ (dB)} = A_{0.01} \left(\frac{p}{0.01} \right)^{-[0.655 + 0.033 \ln(p) - 0.045 \ln(A_{0.01}) - z \sin \theta (1-p)]} \quad (8)$$

where p is the percentage probability of interest and z is given as:

$$\begin{aligned} z &= 0 \text{ if } p \geq 1\%, \\ \text{if } p < 1\%, z &= 0 \text{ for } \varphi \geq 36^\circ \\ z &= -0.005(|\varphi| - 36) \text{ for } \theta \geq 25^\circ \text{ and } |\varphi| < 36^\circ \\ z &= -0.005(|\varphi| - 36) + 1.8 - 4.25 \sin \theta \text{ for } \theta < 25^\circ \text{ and } |\varphi| < 36^\circ \end{aligned} \quad (9)$$

φ and θ are the latitude of the earth station and elevation angle respectively.

3.5. Bryant attenuation model

Derived a model which consisted variables such as the height of rain and the effective rain cell [4]. The model is given by (11)-(19) as shown in:

$$D = 340(R_p^{-1.2}) \text{ [km]} \quad (11)$$

$$D_m = \left(\frac{z}{\pi} \right)^D \quad (12)$$

where R_p is the rain rate. The slant path length (L) can then be calculated as:

$$L = \frac{H_R}{\tan \theta} \quad (13)$$

where: H_R is the rain height and θ is the elevation angle. Estimation of the rain height is done as shown in:

$$H_R \text{ (km)} = 4.5 + 0.0005 R_p^{1.65} \quad (14)$$

where: R_p is the rain rate for the given location. The slant path can then be calculated as shown in:

$$L_s = \frac{H_R - H_s}{\sin \theta} \text{ for } \theta \geq 5^\circ \text{ [km]} \tag{15}$$

and

$$L_s = \frac{2(H_R - H_{HMSL})}{[\sin^2 \theta + 2(H_R - H_{HMSL})/R_E]^{1/2} + \sin \theta} \text{ for } \theta < 5^\circ \text{ [km]} \tag{16}$$

where: H_R and θ height of rain and elevation angle respectively while H_{HMSL} is the height above sea level and R_E is the radius of the earth. Attenuation due to rainfall is hence obtained as:

$$A_{0.01} = 1.57 D_m k_n \gamma R_{0.01} \frac{L_s}{\xi L + D} \text{ for } R_{0.01} > 3 \text{ mm/h} \tag{17}$$

The cross over coefficient denoted k_n is given as:

$$k_n = \exp(0.007 R_p) \tag{18}$$

The cross-over coefficient optimizes the mean diameter of the equivalent single cell over the full rain-rate gauge so that it produces the same attenuation in a given slant path as a set of multiple cells. The Rho factor denoted ξ is given as shown in:

$$\xi = \begin{cases} \frac{1}{\sqrt{2}} \exp(\sin \theta) & \theta \leq 55^\circ \\ 1.1 \tan \theta & \theta > 55^\circ \end{cases} \tag{19}$$

where: θ denotes the elevation angle.

3.6. Svyatogor model

The model developed by [8] is given by (20)-(25) outlined by the following steps:

$$H_R \text{ (km)} = \frac{2.7}{\log_{10}(0.3 R_p + 1.5)} + 0.0015 R_p \tag{20}$$

where: R_p denotes the rain rate. The reduction factor for specific paths is given as:

$$K_{rs} = e^Y \tag{21}$$

where:

$$Y = -0.0045 R_p^{0.68} \left[\frac{H_R}{\tan \theta} \right]^{0.6} \tag{22}$$

With rain attenuation given as:

$$A \text{ (dB)} = k R_p^\alpha L_s K_{rs} \tag{23}$$

where: L_s is the slant path given in (24); K_{rs} is the reduction factor given by (21). k and α are constants obtained from the ITU-R recommendations in [7].

$$L_s \text{ (km)} = \frac{H_R - H_s}{\sin \theta} \text{ for } \theta \geq 5^\circ \tag{24}$$

$$L_s \text{ (km)} = \frac{2(H_R - H_s)}{[\sin^2 \theta + \frac{2(H_R - H_s)}{R_e}]^{1/2} + \sin \theta} \text{ for } \theta < 5^\circ \tag{25}$$

where: R_e is the radius of the earth and is taken as 8500km; H_s is the station height; H_R is the rain height and θ is the elevation angle.

3.7. The ITU-R model

The ITU-R P. 618-9 model [35] is given by (26)-(39) as shown in:

The rain height is denoted H_R where:

$$H_R = h_0 + 0.36 \text{ km} \tag{26}$$

$h_0 = 0^\circ\text{C}$ isotherm height

Estimation of slant path length L_s is given as:

$$L_s = \frac{H_R - H_s}{\sin \theta} \quad (27)$$

with θ and H_s are the elevation angle and station height respectively. The horizontal projection L_G is given as:

$$L_G = L_s \cos \theta \quad (28)$$

The rainfall rate for 99.99% availability can be obtained from rain gauge experiments or rainfall databases for the specific location. The rainfall rate can be given by the following relationship as suggested by the ITU-R P.838-3 recommendations. It is given by:

$$\gamma R_{0.01} = k R_{0.01}^\alpha \quad (29)$$

The constants k and α are gotten from recommendation ITU-R P.838-3 [7]. The next step is to calculate the horizontal reduction factor denoted by $\Gamma_{h0.01}$ for 99.99% availability. The horizontal reduction factor is given as:

$$\Gamma_{h0.01} = \frac{1}{1 + 0.78 \sqrt{\left(\frac{L_G \gamma R_{0.01}}{f}\right) - 0.38 [1 - \exp(-2L_G)]}} \quad (30)$$

where: f = frequency (GHz)

The vertical adjustment factor for 99.99% availability is realized as:

$$L_R = \frac{L_G \Gamma_{0.01}}{\cos \theta} \text{ for } \rho > \theta \quad (31)$$

otherwise,

$$L_R = \frac{H_R - H_s}{\sin \theta}, \text{ for } \rho \leq \theta \quad (32)$$

where:

$$\rho = \tan^{-1} \left(\frac{H_R - H_s}{L_G \Gamma_{h0.01}} \right) \quad (33)$$

therefore,

$$V_{0.01} = \frac{1}{1 + \sqrt{\sin \theta \left[31 \left(1 - \exp\left(-\frac{\theta}{1+\sigma}\right) \right) \frac{\sqrt{L_G \gamma R_{0.01}}}{f^2} - 0.45 \right]}} \quad (34)$$

where:

$$\sigma = 36 - |\varphi|, \text{ for } |\varphi| < 36^\circ \text{ or } \sigma = 0, \text{ for } |\varphi| \geq 36^\circ$$

with φ known to be the latitude of the location the effective path length L_{eff} (km) through rain is calculated as:

$$L_E = L_R V_{0.01} \quad (35)$$

The final step is to estimate the rain attenuation exceeded for 99.99% and is given by:

$$A_{0.01} = \gamma R_{0.01} L_E \quad (36)$$

To calculate for other percentages of time the following expression can be used:

$$A_p(\text{dB}) = A_{0.01} \left(\frac{p}{0.01} \right)^{-[0.655 + 0.033 \ln(p) - 0.045 \ln(A_{0.01}) - z \sin \theta (1-p)]} \quad (37)$$

where p is the percentage probability of interest and z is given by:

$$z = 0 \text{ if } p \geq 1\%$$

$$z = 0 \text{ for } \varphi \geq 36^\circ \text{ if } p < 1\%$$

$$z = -0.005(|\varphi| - 36) \text{ for } \theta \geq 25^\circ \text{ and } |\varphi| < 36^\circ \tag{38}$$

$$z = -0.005(|\varphi| - 36) + 1.8 - 4.25 \sin \theta, \text{ for } \theta < 25^\circ \text{ and } |\varphi| < 36^\circ \tag{39}$$

3.8. Garcia-Lopez attenuation model

In (40) and (41) shows the procedure proposed by [9] for deriving the attenuation due to rainfall and rain heights respectively. The model is given as shown in (40).

$$A = \frac{kR^\alpha L_s}{\left[a + \left\{ \frac{L_s(bR + cL_s + d)}{e} \right\} \right]} \tag{40}$$

The method derived by [9] for attenuation prediction depends on four coefficients. These coefficients are regarded as worldwide coefficients and are useful for determining the attenuation for different percentages of time for an average year. The coefficients of the model are denoted a, b, c, and d with corresponding values of 0.7, 18.35, -16.51, and 2408 respectively. For locations such as Nigeria, the coefficients for a, b, c, and d are 0.72, 7.6, -4.75, and 2408 respectively [20]. k and α are determined as given in [7]. The slant path length is gotten from (27) while the rain height is given as shown in:

$$H_r(\text{km}) = \begin{cases} 4 & 0 < \Psi < 36^\circ \\ 4 - 0.075(|\Psi| - 36^\circ) & \Psi \geq 36^\circ \end{cases} \tag{41}$$

where: Ψ = latitude of earth station

4. RESULTS AND DISCUSSION

4.1. Rainfall distribution of the study area

The study area for the beacon experiment is Longitude 8.88 °E and Latitude 9.91 °N which is a hypothetical location for NIGCOMSAT-1Rs backup station. The location has two seasons which include the dry and wet seasons. The wet or rainy season usually lasts from late March to October while the dry or non-rainy season spans the months of November to February. The rainfall data used in this study is obtained from rain gauge experiments, the tropical rainfall measurement mission, Nigeria environmental, and climatic observatory (NECOP) propagation mission, and validated with the Nigerian meteorological agency (NIMET). The rain gauge experiment and attenuation estimation on the earth-space link lasted for 17 months. The study area experiences small amounts of rain during the dry season due to the tropical continental air mass over the location while the wet season experiences heavier amounts of rain due to the maritime air mass moisture from the South [36]-[44]. The average yearly precipitation for the study location is 1239.20 mm.

4.2. Results for rain attenuation prediction

The estimated rain attenuation obtained for Ku-band at 42.5° elevation angle for the 13 stations using the different attenuation prediction models is compared. Results show that attenuation values predicted gradually decrease with an increase in percentage exceedance. From Figure 2(a), for a system design of 99.99% availability, an attenuation of 0.7399 dB, 12.2015 dB, 21.7352 dB, 31.7040 dB, and 29.8778 dB is predicted by the Svajatorgor, Garcia, ITU-R, the proposed model, and the Bryant model respectively. Since the maximum power of Nigeria's NIGCOMSAT-1R Ku band transponder is 150 w, both the Bryant and proposed model suggest signal outage for 0.01% unavailability. For a system design of 36.5 days/yr to 8.77 hrs/yr unavailability, Figures 2(a)-(d), Figure 3(a)-(d), Figure 4(a) and 4(b), Figure 5(a)-(c) show that all five models estimate the possibility of signal across all thirteen (13) stations. This is because of a signal loss due to rain that ranged from 0.008725 dB (1.002 w) to 8.6743 dB (7.369 w). From Figure 2(b), the Svajatorgor, Garcia, and ITU-R model estimate signal attenuation values of 0.8310 dB (1.211 w), 11.951 dB (15.671 w), 20.1965 dB (104.629 w) which suggests the possibility of signal at 99.99% availability. The proposed model and Bryant model however estimated attenuation values of 26.830 dB (481.948 w) and 26.365 dB (433.052 w) respectively. Both models suggest that the NIGCOMSAT-1R Ku band transponder would require an additional spot beam power of at least 283.052 w to overcome the predicted attenuation. Results from Figure 2(b) further show the possibility of signal at 90% to 99.9% across all models for the thirteen (13)

selected stations. From Figure 2(c), all five models suggest the availability of signal at 90% to 99.9% for the selected station. However, the proposed and Bryant model estimate signal outage for 99.99% availability due to an attenuation estimation of 28.663 dB and 27.683 dB respectively. An attenuation of 0.7955 dB, 11.7815, and 20.78 dB was predicted by the Svajatogor, Garcia, and ITU-R rain models and suggest the availability of signal at 99.99% availability.

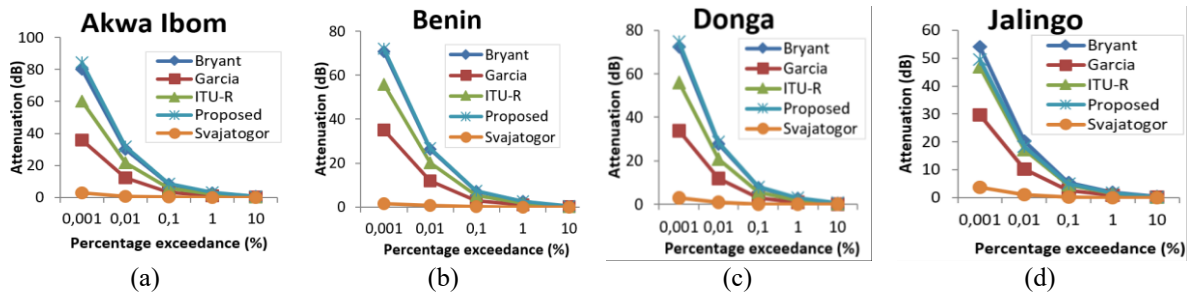


Figure 2. Performance of rain attenuation models in (a) Akwa Ibom, (b) Benin, (c) Donga and (d) Jalingo

Figure 2(c) hence suggests a power shortage of 585.021 w and 436.538 w estimated by the proposed and Bryant rain attenuation prediction models respectively. For a system design of 99.999% availability, only the Svajatogor model suggests the possibility of signal at 99.999% availability. The Garcia, ITU-R, proposed and Bryant model hence estimate additional power requirements of 2207.925 w, 407,746.52 w, 17911269.27 w, and 30408700.25 w respectively for the possibility of signal of 99.999% availability. Results from Figure 2(d) show that for a system design of 53 minutes of outage a year (0.01% unavailability), attenuation values of 1.0175 dB, 10.331 dB, 17.2151 dB, 20.2657 dB, and 18.3427 were realized for the Svajatogor, Garcia, ITU-R Bryant and proposed models respectively. Based on results, signal would be impossible at 99.999% availability as suggested by the Garcia, Bryant, ITU-R, and proposed model. For 99.99% availability, all models suggest the possibility of signal across the selected station. Generally, only the Svajatogor model predicts the possibility of signal at 90% to 99.999% availability. From Figures 3(a) and 3(b), and considering for 99.99% availability, the Bryant model predicted the highest attenuation value of 20.6045 dB and 20.3016 dB for Jos and Makurdi respectively while the proposed model predicted attenuation of 18.8106 dB and 18.3922 dB for the two stations (Jos and Makurdi). All five models suggest the possibility of signal for a system design of 53 minutes of outage a year for the two stations. At time exceedance of 0.001%, signal is impossible across the two stations (Jos and Makurdi) according to all models except that of Svajatogor.

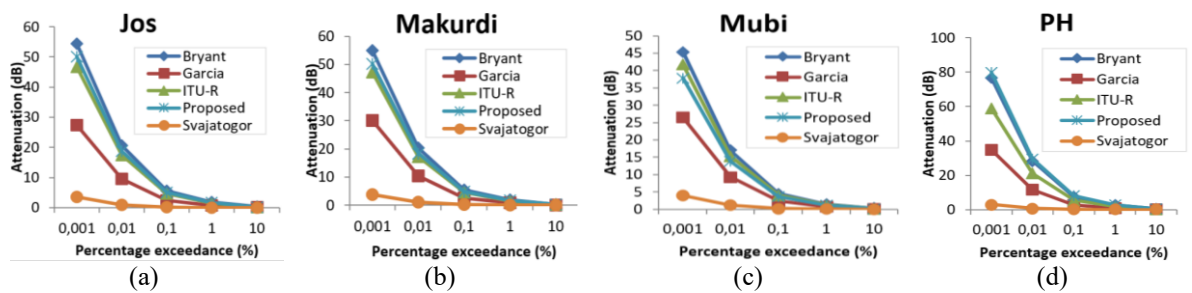


Figure 3. Performance analysis of rain attenuation models in (a) Jos, (b) Makurdi, (c) Mubi and (d) PH

Due to a power requirement of 128.85 w (21.100 dB) necessary in overcoming attenuation due to rain for Mubi station as suggested by the ITU-R model, signal can be said to be possible for 99.99% availability as shown in Figure 3(c). Results on Figures 3(c) and 3(d) further suggest signal unavailability for a system design of 5.26 minutes outage in a year as estimated by the Garcia, ITU-R, proposed and Bryant model. However, Figures 3(c) and 3(d) show that signal is possible at 90% to 99.99% as suggested by the ITU-R, Garcia, and Svajatogor models. From Figure 3(d), the Bryant and proposed model estimate additional Ku band spot beam power of 541.512 w and 773.911 w respectively to overcome the attenuation for Port Harcourt earth station.

From Figure 4(a), only the proposed and Bryant model suggests signal outage for 90% to 99.99% of time. All other models suggest the possibility of signal for the time range. From Figure 4(b), only the Bryant model predicts signal outage for a system design of 53 minutes of outage in a year. This is due to a 12.065 w power shortage resulting in scattering of signals due to rain.

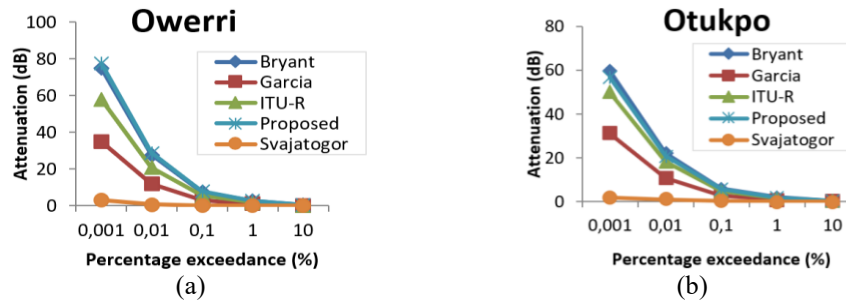


Figure 4. Performance comparison of rain attenuation prediction models (a) Owerri and (b) Otukpo

Attenuation due to rain predicted by all five models for 90% to 99.999% of time ranged from 0.008725 dB to 36.0593 dB for the selected station shown in Figure 5(a). However, signal is possible only at 90% to 99.99% availability. At 0.001% of time, Figure 5(a) shows that the proposed model's attenuation prediction value is lower than that of the ITU-R signifying a trend change in attenuation prediction as results from Figures 2(a)-(d), 3(a)-(d), 4(a) and (b) show that the proposed model estimates higher attenuation values than the ITU-R for higher rainfall rates. The predicted attenuation for the proposed model was 26.0567 dB while that of the ITU-R model was 35.5938 dB. From the results shown in Figure 5(b), attenuation values for 0.01% unavailability ranged from 0.7695 dB to 30.0614 dB across all five models. The attenuation values were 0.7695 dB, 11.556 dB, 21.23 dB, 28.6903 dB, and 30.0614 dB for the Svajatogor, Garcia, ITU-R, Bryant, and proposed model respectively. The signal loss estimates from Figure 5(b) show that signal is possible based on predictions by the Svajatogor, Garcia, and ITU-R model. The Bryant and proposed model however suggest signal outage for 99.99% availability. For a system design of 0.001% unavailability, the proposed model estimated attenuation of 80.4543 dB suggesting total signal outage and a spot beam power exceeding 111027356.596 w to overcome the signal outage. However, for the link availability range of 90% to 99.9% all five models suggest the possibility of signal across the station. Results from Figure 5(c) suggest the possibility of signal for a system design of 99.99% availability across all models for the selected station. For a design of 0.001% unavailability, only the Svajatogor model suggests the possibility of signal. The proposed, Bryant, Garcia, and ITU-R models predicted signal outages across the station. The rain attenuation predicted by the proposed model for Abuja station showed agreement with the results from the work of [39] for Abuja as predicted attenuation due to rain was 19.6018 dB for this study and 18.7135 dB for [39]. The proposed model estimated attenuation at 99.9% to 99.999% for the thirteen cities as shown in Table 1. Sokoto and Aba recorded the lowest and highest attenuation of 9.45 db and 30.06 db for 0.01% respectively.

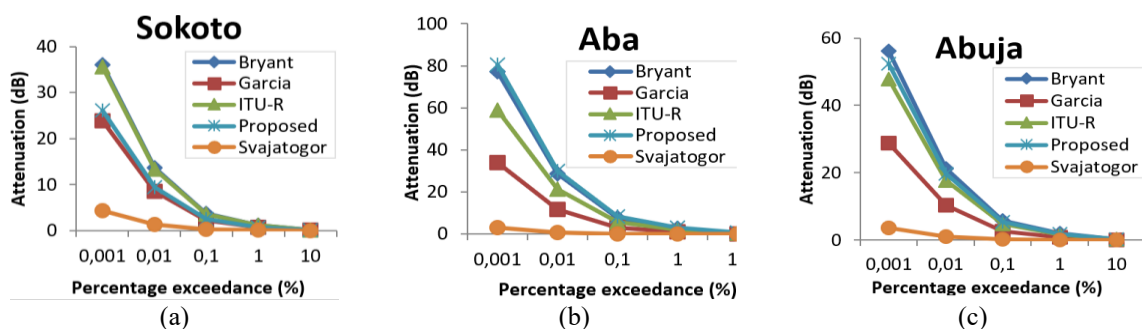


Figure 5. Performance analysis of rain attenuation prediction models (a) Sokoto, (b) Aba, and (c) Abuja

Table 1. Rain attenuation and geometric characteristics of receiver sites

No.	City	0.1%	0.01%	0.001%	Lat/Long	H _s	R _{0.01}
1	Aba	8.198	30.061	80.454	5.12 °N/7.37 °E	205	123.26
2	Abuja	5.323	19.602	52.453	9.07 °N/7.39 °E	360	105.65
3	Akwaibom	8.674	31.704	84.597	4.90 °N/7.85 °E	43	125.75
4	Benin	7.297	26.830	71.928	6.33 °N/5.60 °E	88	118.19
5	Donga	7.990	28.663	74.830	7.75 °N/10.17 °E	344	121.10
6	Jalingo	4.936	18.343	49.536	8.89 °N/11.37 °E	351	103.26
7	Jos	5.128	18.811	50.090	9.89 °N/8.85 °E	1220	104.16
8	Makurdi	4.897	18.392	50.262	7.73 °N/8.53 °E	91	103.35
9	Mubi	3.652	13.806	37.874	10.26 °N/13.26 °E	572	93.92
10	Otukpo	5.601	20.880	56.679	7.19 °N/8.13 °E	170	108.01
11	Owerri	7.867	28.882	77.372	5.48 °N/7.01 °E	75	121.44
12	PH	8.049	29.656	79.773	4.81 °N/7.04 °E	12	122.64
13	Sokoto	2.480	9.451	26.056	13.00 °N/5.24 °E	265	83.48

5. CONCLUSION

This study proposed a new rain attenuation prediction model based on the rain cell concept. The constants used in developing the proposed model were obtained from Ku-band beacon experiments in tropical locations. The proposed model was compared with four other rain attenuation prediction models. The results obtained have shown that the ITU-R P.618 model, Bryant model, Svjatogor model, Garcia model, and the proposed model can be used to predict attenuation due to rain at Ku-band in different selected locations in Nigeria. From the values of attenuation predicted by the proposed model for 99.99% availability, signal is seen to be possible across seven stations. The predicted attenuation values were 18.3427 dB, 18.8106 dB, 18.3921 dB, 13.8062 dB, 20.8803 dB, 9.4519 dB, and 19.6018 dB for Jalingo, Jos, Makurdi, Mubi, Otukpo, Sokoto, and Abuja respectively. However, signal fade-out is predicted across the remaining six stations with predicted attenuation values of 31.7040 dB, 26.8302 dB, 28.6635 dB, 29.6562 dB, 28.8827 dB, and 30.0614 dB for Akwa Ibom, Benin, Donga, Port-Harcourt, Owerri, and Aba respectively. The proposed model hence suggests an additional Ku-band spot beam power of at least 331.97 w to overcome the predicted attenuation across the six stations which recorded signal outage. Since higher frequencies are more prone to attenuation, further studies and models for rain attenuation prediction on Ka-band are required.

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