Physical layer security in hybrid TPSR two-way half-duplex relaying networks over rayleigh fading channel: non-zero secrecy probability analysis

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ABSTRACT

In this paper, we proposed and investigated the Hybrid TPSR Two-Way Half-Duplex (HD) Relaying Communication Networks Over Rayleigh Fading Channel in the presence of the Eavesdropper (E). The system model consists of two sources A and B communicate with each other with helping of intermediate Relay (R). For the system performance analysis, we analyzed and derived the exact and approximate integral-form of the system Non-zero secrecy probability (NZSP) in the case that the E uses the MRC (maximal ratio combining) technique. In addition, the effect of the main system parameters on the system performance is investigated. Finally, all the research results are convinced by the Monte Carlo Simulation. This paper can provide a novel recommendation for relaying communication network manufacture.

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1. INTRODUCTION

Radio frequency (RF) signals with excellent advantages, such as small dimensions, low cost, and independence concerning time and location in urban areas can be considered as electrical sources for cooperative network devices. In addition, RF signals can provide both information and energy in the communication network nodes through a well-known technique in the communication cooperative network called wireless powered networks (WPNs) [1-10]. The security issue is increasingly considered as the main study and improvements in wireless communications, especially the physical layer. Studies on the information exchange security have always been extensively performed for the upper layers, but currently, the security provided in the physical layer has gained significant importance. Physical-layer security (PLS) has recently attracted considerable attention since these approaches can prevent eavesdropping without data encryption in the upper layer [10-18].

In this paper, we proposed and investigated the Hybrid TPSR Two-Way Half-Duplex (HD) Relaying Communication Networks Over Rayleigh Fading Channel in the presence of the Eavesdropper (E). The system model consists of two sources A and B communicate with each other with helping of intermediate Relay (R). For the system performance analysis, we analyzed and derived the exact and approximate integral-form of the system Non-zero secrecy probability (NSP) in the case that the E uses the MRC (maximal ratio combining) technique. In addition, the effect of the main system parameters on the system performance is investigated. Finally, all the research results are convinced by the Monte Carlo Simulation.

2. SYSTEM MODEL

In this section, the system model is drawn in Figure 1 with two sources A and B communicate with each other with helping of intermediate Relay (R) in the presence of the Eavesdropper (E). The energy harvesting (EH) and information processing (IT) of the system model are proposed in Figure 2 as in [19-25].



Figure 1. System model

•	Т	
EH at R $(1-\beta)P_A$	EH at R $(1-\beta)P_B$	IT
$IT: \beta P_A$ $A \longrightarrow R$	$IT: \beta P_B$ $B \longrightarrow R$	$R \longrightarrow A \& B$
<i>α</i> Τ	<i>α</i> Τ	$\rightarrow (1-2\alpha)T$

Figure 2. The EH and IT phases

2.1. Energy harvesting phase

In the first phase αT , A will transmit the message x_A with the power P_A and the signal received at R can be given by:

$$y_{AR} = \sqrt{\beta} h_{AR} x_A + n_R^1 \tag{1}$$

where n_R^1 is additive white Gaussian noise (AWGN) with variance δ_1^2 and h_{AR} is channel gain of A-R link and $E\{|x_A|^2\} = P_A$ in which $E\{\bullet\}$ is the expectation operator.

The EH relay employs a fixed power-splitting factor β to split the received RF power into two parts: $\sqrt{\beta} (h_{AR} x_A + n_R)$ is used for information transmission, and remaining power $\sqrt{1-\beta} (h_{AR} x_A + n_R)$ is used for EH. The amount of harvested energy during the first and second phase can be obtained as:

$$E_{R} = \eta \left(1 - \beta \right) \alpha T \left(P_{A} \left| h_{AR} \right|^{2} + P_{B} \left| h_{BR} \right|^{2} \right)$$
⁽²⁾

where $0 < \eta \le 1$ is energy conversion efficiency, P_B is the average transmitted power at the source B, and h_{BR} are the channel gain of B-R link. Moreover, $0 \le \beta < 1$ and $0 \le \alpha < 0.5$ is the power splitting and time-switching factor, respectively. We assume that $P_A = P_B = P$, (2) can be rewritten as

$$E_{R} = \eta \left(1 - \beta\right) \alpha TP \left(\left|h_{AR}\right|^{2} + \left|h_{BR}\right|^{2}\right)$$
(3)

The average transmitted power at the relay can be obtained as:

$$P_{R} = \frac{E_{R}}{T(1-2\alpha)} = \frac{\eta(1-\beta)\alpha TP(|h_{AR}|^{2}+|h_{BR}|^{2})}{T(1-2\alpha)} = \kappa P(|h_{AR}|^{2}+|h_{BR}|^{2})$$
(4)

 $\kappa = \frac{\eta(1-\beta)\alpha}{1-2\alpha}$

where

2.2. Information transmission phase

In the first phase, after doing EH, A will broadcast the information to relay node and B with remaining power βP_A . Hence, the received signal at R can be expressed as, respectively.

$$y_{AR} = \sqrt{\beta} h_{AR} x_A + n_R^1 \tag{5}$$

Similar to the first phase, the received signal at R can be given in the second phase,

$$y_{BR} = \sqrt{\beta} h_{BR} x_B + n_R^2 \tag{6}$$

where h_{BR} is channel gain of B-R link and $E\{|x_B|^2\} = P_B$ and n_R^2 is AWGN with variance δ_2^2 Hence, the total received signal at R after A and B node transmit their signal can be expressed by:

$$y_R = \sqrt{\beta} h_{AR} x_A + \sqrt{\beta} h_{BR} x_B + n_R \tag{7}$$

where $n_R = n_R^1 + n_R^2$ denoted the total AWGN at R with variance N₀. Finally, in the third phase, the received signal at A and B node can be expressed as, respectively.

$$y_A = h_{RA} x_R + n_A,$$

$$y_B = h_{RB} x_R + n_B$$
(8)

where h_{RA} , h_{RB} is channel gain of R-B link and R-A link, respectively, n_A , n_B is AWGN with variance N₀ at A and B node and $E\{|x_R|^2\} = P_R$. In our proposed model, we will consider amplify and forward (AF) mode. In order to ensure that the transmission power at *R* is P_R, the amplifying coefficient μ can be chosen as,

$$\mu = \frac{x_R}{y_R} = \sqrt{\frac{P_R}{\beta \left[P_A \left| h_{AR} \right|^2 + P_B \left| h_{BR} \right|^2 \right] + N_0}} = \sqrt{\frac{P_R}{\beta P \left[\left| h_{AR} \right|^2 + \left| h_{BR} \right|^2 \right] + N_0}}$$
(9)

From (7) and combine with (5), (6), the received signal at A node can be rewritten as,

$$y_{A} = h_{RA} \mu (y_{AR} + y_{BR}) + n_{A}$$
(10)

Substituting (7) into (10), we can obtain as follows:

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$$y_{A} = h_{RA} \mu \left(\sqrt{\beta} h_{AR} x_{A} + \sqrt{\beta} h_{BR} x_{B} + n_{R} \right) + n_{A} = h_{AA} \mu \sqrt{\beta} h_{BR} x_{B} + h_{A} \mu \sqrt{\beta} h_{A$$

This signal contains both messages x_A and x_B , while only x_B is the desired signal at A. Since node A perfectly knows its own transmitted symbol x_A , it can eliminate the corresponding the self-interference term $h_{RA}\mu\sqrt{\beta}h_{AR}x_A$ from y_A Therefore, equation (11) can be rewritten by

The signal to noise ratio (SNR) at A node can be calculated by:

$$\gamma_{A} = \frac{\mathrm{E}\left\{\left|signal\right|^{2}\right\}}{\mathrm{E}\left\{\left|noise\right|^{2}\right\}} = \frac{\left|h_{RA}\right|^{2}\left|h_{BR}\right|^{2}\mu^{2}\beta P}{\left|h_{RA}\right|^{2}\mu^{2}N_{0} + N_{0}}$$
(13)

Substituting (5) into (9) and then doing some algebra, we have:

$$\gamma_A \approx \frac{\kappa \beta \Psi \left| h_{RA} \right|^2 \left| h_{BR} \right|^2}{\kappa \left| h_{RA} \right|^2 + \beta}$$
(14)

 $\Psi = \frac{P}{N_0}$ where

In the total information transmission phase, while R will receive both legitimated message x_A and x_B from source node A and B, E will also overhear the information transmitted by A and B node. Thus, the received signal at E can be obtained as

$$y_{E}^{1} = h_{AE}x_{A} + h_{BE}x_{B} + n_{E}$$
(15)

where h_{AE} , h_{BE} are the channel gain of A-E and B-E links, respectively and n_E is AWGN with variance N₀. During the broadcast signal phase, E also overhears the information from R. Hence, the received signal at E can be given by

$$y_{E}^{2} = h_{RE} x_{R} + n_{E} = h_{RE} \mu y_{R} + n_{E}$$
$$= h_{RE} \mu \left(\sqrt{\beta} h_{AR} x_{A} + \sqrt{\beta} h_{BR} x_{B} + n_{R} \right) + n_{E}$$
(16)

In our model, we will analyze the intercept (IP), non-zero secrecy (NZSP) and secrecy outage probability (SOP) at node A because our system model is symmetry and we can analyze at node A or node B. Therefore, from (15) and (16), the SNR at E to decode successful message of node A in two different phases can be claimed as, respectively.

$$\gamma_E^1 = \frac{|h_{AE}|^2 P_A}{|h_{BE}|^2 P_B + N_0} = \frac{|h_{AE}|^2 \Psi}{|h_{BE}|^2 \Psi + 1}$$
(17)

$$\gamma_{E}^{2} = \frac{|h_{RE}|^{2} \mu^{2} \beta |h_{AR}|^{2} P_{A}}{|h_{RE}|^{2} \mu^{2} \beta |h_{BR}|^{2} P_{B} + |h_{RE}|^{2} \mu^{2} N_{0} + N_{0}} \approx \frac{\beta |h_{AR}|^{2} P_{A}}{\beta |h_{BR}|^{2} P_{B} + N_{0}} = \frac{\beta |h_{AR}|^{2} \Psi}{\beta |h_{BR}|^{2} \Psi + 1}$$
(18)

3. SYSTEM PERFORMANCE ANALYSIS

With MRC technique, E combines SNR from (17) and (18). Hence, the end to end SNR at E can be obtained by

$$\gamma_{E}^{MRC} = \gamma_{E}^{1} + \gamma_{E}^{2} = \frac{\left|h_{AE}\right|^{2} \Psi}{\left|h_{BE}\right|^{2} \Psi + 1} + \frac{\beta \left|h_{AR}\right|^{2} \Psi}{\beta \left|h_{BR}\right|^{2} \Psi + 1}$$
(19)

From (14) and (19), we can claim the capacities at nodes A and E, respectively.

$$C_{A} = \frac{(1-2\alpha)T}{3} \times \log_{2} \left(1+\gamma_{A}\right),$$

$$C_{E}^{MRC} = \frac{(1-2\alpha)T}{3} \times \log_{2} \left(1+\gamma_{E}^{MRC}\right)$$
(20)

3.1. Non-zero secrecy probability (NZSP) analysis

From (20), the secrecy capacity can be obtained by

$$C_{e2e}^{\text{Sec}} = \max\left[0, C_A - C_E^{MRC}\right]$$
(21)

The NZSP of the system can be formulated as followings after combine with (14) and (19):

$$NZSP = \Pr\left(C_{e^{2}e}^{Sec} > 0\right) = \Pr\left(C_{A} > C_{E}^{MRC}\right) = \Pr\left(\gamma_{A} > \gamma_{E}^{MRC}\right)$$
$$= \Pr\left(\frac{\kappa\beta\Psi\left|h_{RA}\right|^{2}\left|h_{BR}\right|^{2}}{\kappa\left|h_{RA}\right|^{2} + \beta} > \frac{\left|h_{AE}\right|^{2}\Psi}{\left|h_{BE}\right|^{2}\Psi + 1} + \frac{\beta\left|h_{AR}\right|^{2}\Psi}{\beta\left|h_{BR}\right|^{2}\Psi + 1}\right)$$
$$= \int_{0}^{\infty} \Pr\left(\gamma_{E}^{MRC} < \gamma_{A}^{e}\right) f_{\left|h_{BR}\right|^{2}}(y)dy$$
(22)

where
$$\mathscr{P}_{E}^{MRC} = \frac{\left|h_{AE}\right|^{2}\Psi}{\left|h_{BE}\right|^{2}\Psi+1} + \frac{\beta\left|h_{AR}\right|^{2}\Psi}{\beta y\Psi+1}$$
 and $\mathscr{P}_{A} = \frac{\kappa\beta\Psi\left|h_{RA}\right|^{2}y}{\kappa\left|h_{RA}\right|^{2}+\beta}$

3.2. Lemma 1. Exact analysis for NZSP

In (22), we have to define $\Pr\left(\mathscr{P}_{E}^{MRC} < \mathscr{P}_{A}\right)$

$$\Pr\left(\mathscr{Y}_{E}^{MRC} < \mathscr{Y}_{A}\right) = \int_{0}^{\infty} F_{\mathscr{Y}_{E}^{MRC}}\left(\mathscr{Y}_{A} \mid \mathscr{Y}_{A} = x\right) f_{\mathscr{Y}_{A}}(x) dx$$

$$(23)$$

The CDF of $\frac{\mathcal{M}^{RC}}{\mathcal{L}}$ and PDF of $\frac{\mathcal{M}}{\mathcal{L}}$ can be calculated by:

$$F_{g_{E}^{ARC}}(x) = \Pr\left(g_{E}^{ARC} < x\right) = \Pr\left(\frac{|h_{AE}|^{2} \Psi}{|h_{BE}|^{2} \Psi + 1} + \frac{\beta |h_{AR}|^{2} \Psi}{\beta y \Psi + 1} < x\right)$$
$$= \Pr\left(X + g_{0}^{A} < x\right) = \int_{0}^{x} F_{X} \left(x - g_{0}^{A}\right) g_{0}^{A} = t \int_{g_{0}}^{x} f_{X}(x - g_{0}^{A}) g_{0}^{A} = t \int_{g_{0}}^{x} f_{Y}(x - g_{0}^{$$

 $X = \frac{\left|h_{AE}\right|^{2} \Psi}{\left|h_{BE}\right|^{2} \Psi + 1} \text{ and } \mathcal{D} = \frac{\beta \left|h_{AR}\right|^{2} \Psi}{\beta y \Psi + 1}$

In (24), the CDF of X and $\frac{1}{2}$ can be computed as, respectively.

$$F_{X}(x) = \Pr\left(X < x\right) = \Pr\left(\frac{|h_{AE}|^{2}\Psi}{|h_{BE}|^{2}\Psi + 1} < x\right)$$

$$= \Pr\left(\left|h_{AE}\right|^{2} < x\left|h_{BE}\right|^{2} + \frac{x}{\Psi}\right) = \int_{0}^{\infty} F_{|h_{AE}|^{2}}\left(x\left|h_{BE}\right|^{2} + \frac{x}{\Psi}\right) \left|h_{BE}\right|^{2} = t\right) \times f_{|h_{BE}|^{2}}(t)dt$$

$$= 1 - \lambda_{BE} \times \exp\left[-\frac{\lambda_{AE}x}{\Psi}\right] \int_{0}^{\infty} \exp\left(-\lambda_{BE}t\right) \times \exp\left(-x\lambda_{AE}t\right)dt$$

$$= 1 - \frac{\lambda_{BE} \times \exp\left[-\frac{\lambda_{AE}x}{\Psi}\right]}{\lambda_{BE} + x\lambda_{AE}}$$
(25)

$$F_{pb}(t) = \Pr\left(\hat{\mathbf{Y}}_{0}(t) = \Pr\left(\frac{\beta |h_{AR}|^{2} \Psi}{\beta y \Psi + 1} < t\right) = \Pr\left(\left|h_{AR}\right|^{2} < \frac{t(\beta y \Psi + 1)}{\beta \Psi}\right)$$
$$= 1 - \exp\left(-\frac{\lambda_{AR}t(\beta y \Psi + 1)}{\beta \Psi}\right)$$
(26)

Applying result from (25) and (26), we have as followings:

$$F_{X}(x-t) = 1 - \frac{\lambda_{BE} \times \exp\left[-\frac{\lambda_{AE}(x-t)}{\Psi}\right]}{\lambda_{BE} + (x-t)\lambda_{AE}}$$
(27)

$$f_{\#}(t) = \frac{\partial F_{\#}(t)}{\partial t} = \frac{\lambda_{AR}(\beta y \Psi + 1)}{\beta \Psi} \times \exp\left(-\frac{\lambda_{AR}t(\beta y \Psi + 1)}{\beta \Psi}\right)$$
(28)

Substituting (27) and (28) into (24):

$$F_{g_{E}^{MBC}}\left(x\right) = \frac{\lambda_{AR}(\beta y\Psi + 1)}{\beta\Psi} \int_{0}^{x} \left\{ 1 - \frac{\lambda_{BE} \times \exp\left[-\frac{\lambda_{AE}(x-t)}{\Psi}\right]}{\lambda_{BE} + (x-t)\lambda_{AE}} \right\} \times \exp\left(-\frac{\lambda_{AR}t(\beta y\Psi + 1)}{\beta\Psi}\right) dt$$
$$= 1 - \exp\left(-x \times r(y)\right) - r(y) \int_{0}^{x} \frac{\lambda_{BE} \times \exp\left[-\frac{\lambda_{AE}(x-t)}{\Psi}\right] \times \exp\left(-\frac{\lambda_{AR}t(\beta y\Psi + 1)}{\beta\Psi}\right)}{\lambda_{BE} + (x-t)\lambda_{AE}} dt$$
$$= 1 - \exp\left(-x \times r(y)\right) - \frac{\lambda_{BE}}{\lambda_{AE}}r(y) \exp\left(-\frac{\lambda_{AE}x}{\Psi}\right) P_{3}$$
(29)

where
$$r(y) = \frac{\lambda_{AR}(\beta y \Psi + 1)}{\beta \Psi}$$
 and $([2 \lambda])$

$$P_{3} = \int_{0}^{x} \frac{\exp\left(-t\left\lfloor r(y) - \frac{\lambda_{AE}}{\Psi}\right\rfloor\right)}{\frac{\lambda_{BE}}{\lambda_{AE}} + (x-t)} dt = \int_{0}^{x} \frac{\exp\left(-t \times \Re(y)\right)}{g(x) - t} dt$$

$$= \exp\left(-\Re(y)g(x)\right) \times \operatorname{Ei}\left(\Re(y)g(x) - t \times \Re(y)\right) \Big|_{X}^{0}$$

$$= \exp\left(-\Re(y)g(x)\right) \times \left[\operatorname{Ei}\left(\Re(y)g(x)\right) - \operatorname{Ei}\left(\Re(y)g(x) - x \times \Re(y)\right)\right]$$
(30)

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Next, we find the CDF of \mathcal{H}_A as follows

$$F_{\mathcal{H}_{A}}(x) = \Pr\left(\mathcal{H}_{A} < x\right) = \Pr\left(\frac{\kappa\beta\Psi\left|h_{RA}\right|^{2} y}{\kappa\left|h_{RA}\right|^{2} + \beta} < x\right)$$

$$= \begin{cases} \Pr\left(\left|h_{RA}\right|^{2} < \frac{x\beta}{\kappa\left(\beta\Psi y - x\right)}\right), y > \frac{x}{\beta\Psi} \\ 1, y \le \frac{x}{\beta\Psi} \end{cases}$$

$$= \begin{cases} 1 - \exp\left[-\frac{\lambda_{RA}x\beta}{\kappa\left(\beta\Psi y - x\right)}\right], x < \beta\Psi y \\ 1, y \le \beta\Psi y \end{cases}$$
(31)

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where λ_{RA} are mean of RV $\left|h_{RA}\right|^2$

From (31), the PDF of $\tilde{\gamma}_A$ can be computed by

$$f_{\frac{\beta}{\beta}}(x) = \frac{\partial F_{\frac{\beta}{\beta}}(x)}{\partial x} = \begin{cases} \frac{\lambda_{RA}\beta^2 \Psi y}{\kappa (\beta \Psi y - x)^2} \times \exp\left[-\frac{\lambda_{RA}x\beta}{\kappa (\beta \Psi y - x)}\right], x < \beta \Psi y\\ 0, x \ge \beta \Psi y \end{cases}$$
(32)

Substituting (29) and (32) into (23), we obtain:

$$\Pr\left(\mathscr{P}_{E}^{\mathcal{MRC}} < \mathscr{P}_{A}\right) = \int_{0}^{\beta \Psi y} F_{\mathscr{P}_{A}^{\mathcal{MRC}}}(\mathscr{P}_{A} \mid \mathscr{P}_{A} = x) f_{\mathscr{P}_{A}}(x) dx$$
$$= \int_{0}^{\beta \Psi y} \left\{ 1 - \exp\left(-x \times r(y)\right) - \frac{\lambda_{BE}}{\lambda_{AE}} r(y) \exp\left(-\frac{\lambda_{AE} x}{\Psi}\right) P_{3} \right\}$$
$$\times \frac{\lambda_{RA} \beta^{2} \Psi y}{\kappa \left(\beta \Psi y - x\right)^{2}} \times \exp\left[-\frac{\lambda_{RA} x \beta}{\kappa \left(\beta \Psi y - x\right)}\right] dx$$
(33)

Substituting (33) into (22); finally we claim as:

$$NZSP = \int_{0}^{\beta\Psi y} \left\{ 1 - \exp\left(-x \times r(y)\right) - \frac{\lambda_{BE}}{\lambda_{AE}} r(y) \exp\left(-\frac{\lambda_{AE}x}{\Psi}\right) P_{3} \right\}$$
$$NZSP = \int_{0}^{\infty} \frac{\lambda_{BR} \lambda_{RA} \beta^{2} \Psi y}{\kappa \left(\beta\Psi y - x\right)^{2}} \times \exp\left[-\frac{\lambda_{RA} x \beta}{\kappa \left(\beta\Psi y - x\right)} - \lambda_{BR} y\right] dxdy$$
(34)

3.3. Lemma 2. Asymptotic analysis for NZSP

At high SNR regime, (24) can be reformulated by

$$F_{\mathcal{H}_{-\infty}^{MRC}}(x) = \Pr\left(\mathcal{H}_{E_{-\infty}}^{MRC} < x\right) = \Pr\left(\frac{|h_{AE}|^{2}}{|h_{BE}|^{2}} + \frac{|h_{AR}|^{2}}{y} < x\right)$$

$$= \Pr\left(\mathcal{H} + \mathcal{H} < x\right) = \int_{0}^{x} F_{\mathcal{H}}(x - \mathcal{H}) \mathcal{H} = t) f_{\mathcal{H}}(t) dt$$
(35)

$$X = \frac{|h_{AE}|^2}{|h_{BE}|^2}, Y = \frac{|h_{AR}|^2}{y}$$

where

The CDF of $\frac{1}{2}$ can be obtained as

$$F_{\mathfrak{H}}(x) = 1 - \frac{\lambda_{BE}}{\lambda_{BE} + x\lambda_{AE}}$$
(36)

The CDF and PDF of \mathcal{P} can be computed as followings, respectively

$$F_{\mathfrak{g}\mathfrak{h}}(t) = \Pr\left(\left|\mathcal{H}_{AR}\right|^{2} < yt\right) = 1 - \exp(-\lambda_{AR}yt),$$

$$f_{\mathfrak{g}\mathfrak{h}}(t) = \lambda_{AR}y\exp(-\lambda_{AR}yt)$$
(37)

Substituting (36), (37) into (35), we have:

$$F_{\mathcal{P}_{E_{\infty}}^{MBC}}\left(x\right) = \int_{0}^{x} \left\{ 1 - \frac{\lambda_{BE}}{\lambda_{BE} + (x - t)\lambda_{AE}} \right\} \lambda_{AR} y \exp(-\lambda_{AR} yt) dt$$
$$= 1 - \exp(-\lambda_{AR} xy) - \frac{\lambda_{BE} \lambda_{AR} y P_{3}^{\prime 0}}{\lambda_{AE}}$$
(38)

where

$$\begin{aligned} & \mathcal{P}_{3}^{c} = \int_{0}^{x} \frac{\exp(-\lambda_{AR} yt)dt}{g(x) - t} = \exp(-\lambda_{AR} yg(x)) \times \operatorname{Ei}(\lambda_{AR} yg(x) - \lambda_{AR} yt) \Big|_{x}^{0} \\ &= \exp(-\lambda_{AR} yg(x)) \times \left[\operatorname{Ei}(\lambda_{AR} yg(x)) - \lambda_{AR} y \times \operatorname{Ei}\left(\frac{\lambda_{BE}}{\lambda_{AE}}\right)\right] \end{aligned}$$

Similar as exact case, we can obtain:

$$NZSP^{\infty} = \int_{0}^{\infty} \int_{0}^{\beta \Psi y} \left\{ 1 - \exp(-\lambda_{AR} xy) - \frac{\lambda_{BE} \lambda_{AR} y P_{3}}{\lambda_{AE}} \right\} \times \frac{\lambda_{BR} \lambda_{RA} \beta^{2} \Psi y}{\kappa (\beta \Psi y - x)^{2}} \times \exp\left[-\frac{\lambda_{RA} x \beta}{\kappa (\beta \Psi y - x)} - \lambda_{BR} y \right] dxdy \quad (29)$$

4. NUMERICAL RESULTS AND DISCUSSION

The influence of α on the system NZSP is illustrated in Figure 3. In this stage, we set the main system parameters as η =0.8, β =0.5 and ψ =5, 10 dB, respectively. From the simulation results, we can state that the NZSP of the model system has a massive increase with the rising of α from 0.05 to 0.45. Furthermore, the NZSP is considered as the function of β , as shown in Figure 4. Here we set α =0.3, ψ =5 dB, and η =0.5, 0.8, respectively. We vary β from 0 to 1 as shown in Figure 4. As shown in Figure 4, NZSP increases when β rises from 0 to 0.4, after the optimal value, the NZSP has a huge decrease when β varies from 0.4 to 1. The maximum value of the system NZSP obtained with β from 0.4 to 0.5. From Figure 4 and Figure 5, we can see that the analytical and the simulation curves are the same to verify the correctness of the system performance analysis section.

Finally, the system NZSP versus η and ψ are considered in Figure 5 and Figure 6, respectively. In Figure 5, we set α =0.3, β =0.5 and ψ =5, 10 dB, and in Figure 6, we set α =0.3, β =0.5, respectively. From Figure 5 and Figure 6, it can be observed that the system NZSP has a massive increase with rising η from 0 to 1 and ψ from 0 to 40 dB, respectively. In addition, the simulation and analytical values of the system NZSP agree with each other to convince the performance analysis section.

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Figure 5. NZSP versus n

0.15

0.1

0.05

0 0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9

In this paper, we proposed and investigated the Hybrid TPSR Two-Way HD Relaying Communication Networks over Rayleigh Fading Channel in the presence of the Eavesdropper (E). For the system performance analysis, we analyzed and derived the exact and approximate integral-form of the system Non-zero secrecy probability (NSP) in the case that the E uses the MRC (maximal ratio combining) technique. In addition, the effect of the main system parameters on the system performance is investigated. Finally, all the research results are convinced by the Monte Carlo Simulation. This paper can provide a novel recommendation for relaying communication network manufacture.

0.5

0.4 0.3

0.2 lon

0

10

5

15

20

 Ψ (dB)

Figure 6. NZSP versus ψ

30

25

40

35

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