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A coplanar waveguide tapered slot antenna with beam switching capabilities

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ABSTRACT

A wideband tapered slot antenna (TSA) with three radiating elements for beam switching purpose is presented in this paper. The integrated radiating taper slots in assistance with metal strips acting as switches provided the proposed design with the capability of switching its beam into three different directions while maintaining the antenna performance stable. To verify the accuracy of the presented design, the prototype was fabricated and measurements were conducted in terms of scattering parameter (S11), radiation pattern and realized gain towards the three different operating modes. By sequentially, activating the switches, the antenna main beam rotated 90º in the XY coordinates. A realized gain ranging from 4.3 to 6.4 dBi and a wide operating bandwidth ((S11) ≤-10 dB) from 3.3GHz to 5GHz were observed throughout the antenna performance in simulation as well as in experiment. With the covered bands, the proposed antenna is suitable for sub-6GHz communications systems.

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1. INTRODUCTION

Whilst the advancement of wireless communication systems increases tremendously, diverse steps are required to tackle the exponential growth in broadband demands. Fixed antennas are limited in performance and unable to cope in a dynamic environment. Reconfigurable antennas were introduced to allocate the antenna beam on the target thus, increase the overall data rate and reduce the interference. Reconfigurable antennas are described as antennas that support multiple functions within a single structure. This reconfiguration comes in different form such as frequency reconfiguration, polarization reconfiguration and pattern reconfiguration depending on the required applications [1-7].

In a dynamic environment, avoiding interferences in a wireless system is crucial, such that directive antenna with switched beam ability are required in such situation to improve the communication linkage by ensuring the signal reaches the intended users. This enables effective and consistent communication for fast-moving information transmitting in both base stations and user terminals of wireless systems [8-11]. Towards achieving beam switching, various approaches have been studied, namely digital beam forming [12-15]. However, this approach is limited to narrow operating band and quite complex. The current approaches are parasitic tuning and multiple radiators, which are widely employed due to the ease of integration [16-22]. In this work, switched radiators approach is proposed to provide a wide tilt angle of ±90° over a wide operating band and a portion of common area is overlapped for miniaturized profile. The beams are configured by channelling the current flows to the radiating slot. The proposed structure conquered the limitation of ±40° in the tilt angle as reported in [23-25]. The existing studies shows that with a wide operating bandwidth, the beam switching directions are limited to two states at the highest gain of 6 dBi [26, 27].

Contrary to the previous works, the proposed structure presents a trade-off between bandwidth coverage and beam switching states with three directive beams at the peak gain of 6.4dBi. An exception is exhibited in [28] with 16 states, every 22.5° covering a narrow bandwidth at the peak gain of 6.2dBi. Nevertheless, the design proposed in this work is a good candidate for wide-beam steering applications. The merits of the proposed structure over previous reported works is the fact that different modes can be combined to boost the reconfigurable states (from 3 states to 7 states without additional switches) and improve the directivity. However, this will be examined in the next study.

2. DESIGN AND EXPERIMENT

The proposed TSA is built from an original TSA with one radiating element. The design is optimized with additional taper slots to increase the reconfigurable states. The proposed design and its parameters is displayed in Figure 1 and Table 1. The top layer engraves three taper slots radiators whereas the lower patch of the antenna grooves of a cpw feed and delay slot-line for wideband matching purpose. An FR4 with 0.8mm of substrate thickness board is used with a relative permittivity of 4.3 and a tangent loss of 0.025. The characteristic impedance was selected to be 50 Ω. Initially, the energy is conveyed from CPW to radiating- slot by a delay slot-line with a basic role of upholding the electric field in phase with the other slot-line. Towards the end of the delay slot-line, the two electric fields stayed in phase for wide transmission capacity to be acquired. Secondly, the wave propagations are directed by the taper slot respecting the orientation of the switched radiator. The fabricated prototypes are depicted in Figure 2.

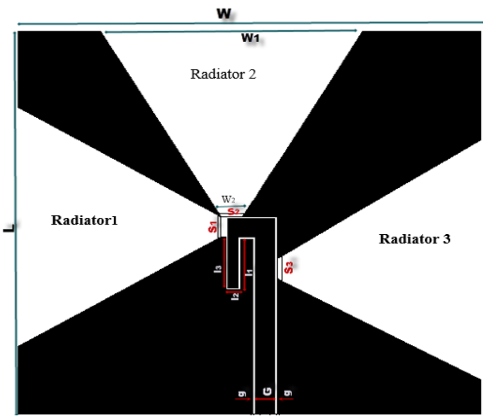


Figure 1. Proposed antenna design structure

Table 1. Optimized parameters of the designed antenna

Variable	Dimension (mm)
W	112.84
W_1	63.8
W_2	5.39
L	102
l_1	13.39
l_2	2.48
l_3	13.95
G	4.84
g	0.56
$S_{1,2,3}$	5.39

In order to achieve the three different modes, the metals strips acted as switches, ideally, for radiator 1 to operate, S_1 is open whereas S_2 and S_3 are short-circuited meaning that metal strips are added on to prevent the current to flow in to the radiator 2 and 3. On the other hand, S_1 and S_3 are short-circuited blocking the current in the left and right modes and allowing the up mode to radiate. Whereas for right mode to be functional, S_1 and S_2 should be short-circuited.

Figure 2. Fabricated prototype with metal strips in up, left and right mode

3. RESULTS AND ANALYSIS

In this study, performance evaluation as technical result style is implemented. The designed antenna as shown in Figure 1 was simulated using computer simulation technology (CST), fabricated and measured to rationalize the accuracy of the proposed beam tilt technique. The performance of the antenna in terms of reflection coefficient was measured using E5071C network analyzer while the radiation patterns were carried out in a SATIMO anechoic chamber.

The feed transition is a major criteria for wideband operation. In this work, the introduction of delay line between radiating slot and CPW was used to provide a broader matching. Overall, a good matching under the condition ($S_{11} \leq |-10|$ dB) from 3.3GHz to 5GHz is observed, this implies that 90% of signal was transmitted with 10% being reflected. Figure 3 highlights the return loss curves base on the switched radiating slot. A shift of 100MHz is observed as the radiating slot moves farther from the delay line. This discrepancy is probably due to the delay matching slot-line, however, the wideband is preserved.

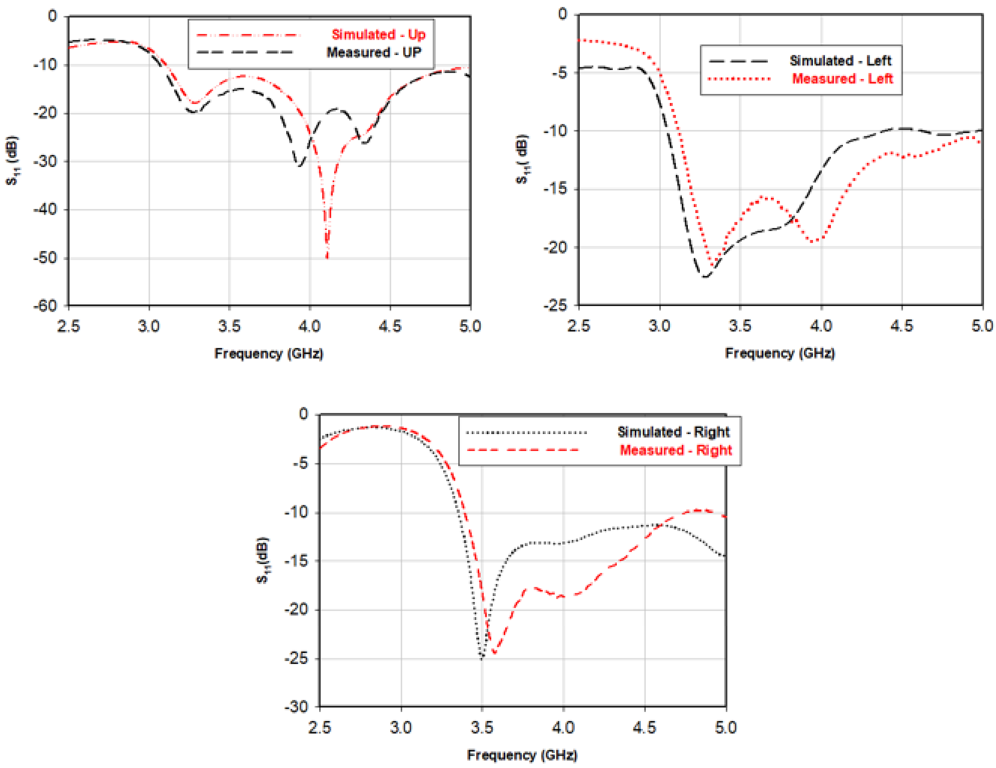
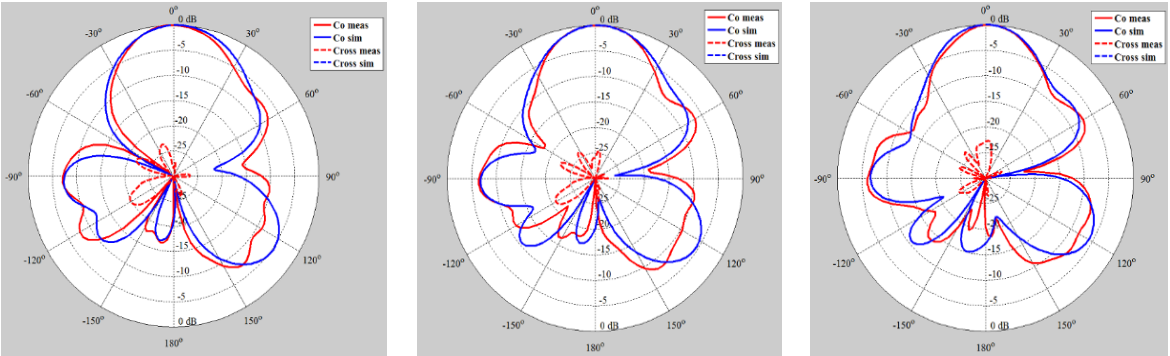


Figure 3. Simulated vs measured S_{11} in up, left and right mode

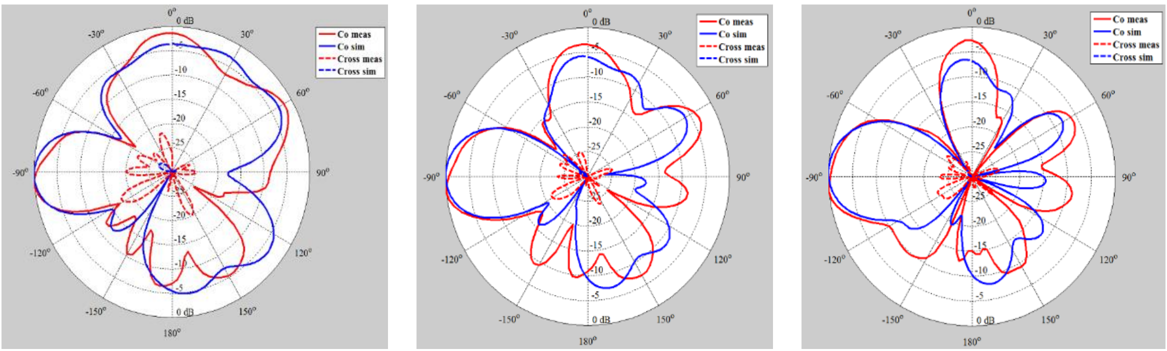
Based on the theory guiding TSA, the beam direction depends on the orientation of the radiators, the beam angle can simply be adjusted if the orientation of the radiator is changed. In this work, the beam can be configured by channelling the current flows to the radiating slot. This technique is flexible, reduces interference from unwanted source and allow increased performance over dipole antennas or omnidirectional antennas. The capacity of the antenna to switch the main beam towards the intended directions while covering a wide tilt angle ±90° is assessed in the XY coordinates and fitted the main objective of this study. A good agreement is observed between measurement and simulation for the three different directions at three different operating frequencies.

It can be seen from Figure 4, at the three examined frequencies, the primary lobe is obtained at phi equals to 0º with less side lobes in the up mode with fixed theta at 90º for the E-phi component in the XY coordinates. By short-circuiting S_2 and S_3, the current flows towards the left mode, as results, the main lobe switched from phi equals to 0º to phi equals to -90º as depicted in Figure 5. The same method is applied to direct the current to the right mode as shown in Figure 6 by opening S_3. Consequently, the pattern beams are controlled. It is observed that the gain does not change dramatically for the three modes with a peak gain of 6.4dBi and a minimum gain of 4.3dBi. The proposed structure rises above the limitation of ±40° in the tilt angle as reported in [23-25]. This research work is based on a tapered slot antenna known as a directive antenna with end-fire characteristics and symmetric pattern in both co-and cross-polarization.



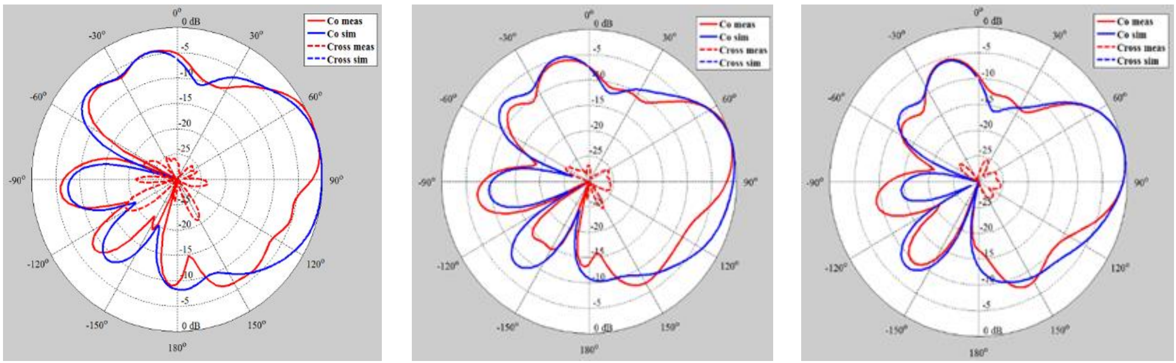
(a) (b) (c)

Figure 4. E-phi component co and cross (sim vs meas)-up mode (a) 3.4GHz, (b)3.6GHz, (c) 3.8GHz



(a) (b) (c)

Figure 5. E-phi component co and cross (sim vs meas)- left mode (a) 3.4GHz, (b)3.6GHz, (c) 3.8GHz



(a) (b) (c)

Figure 6. E-phi component co and cross (sim vs meas)-right mode (a) 3.4GHz, (b)3.6GHz, (c) 3.8GHz

4. CONCLUSION

A wideband tapered slot antenna with beam switching capabilities is presented in this monograph. The viability of switching the main beam with respect to the intended directions not affecting its operating bandwidth was evaluated. The proposed design achieved three different directions with a realized gain ranging from 4.3 to 6.4dBi. The total efficiency varies from 92% in simulation to 60% in experiments. Furthermore, it is suggested to explore the performance of the design in active mode without the increment in size and the disturbance in the pattern.

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