Outage probability analysis of DF PSR energy harvesting Full-Duplex relaying network with presence of the direct link using MRC technique

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Article Info

Article history:

Received Jan 26, 2019 Revised Apr 22, 2019 Accepted May 7, 2019

Keywords:

Decode-and-forward (DF) Energy harvesting (EH) Outage probability (OP) Power splitting protocol (PS) Relaying network

ABSTRACT

In the last time, the system performance of the energy harvesting relay network has been considered in many studies. In this paper, we propose and investigate the outage probability (OP) of the Decode-and-Forward (DF) Energy Harvesting (EH) Full-Duplex (FD) Relaying network in Power Splitting Protocol (PS) using MRC Technique with the presence of the direct link. In the first stage, the integral form of the OP is derived in two cases with and without the presence of the direct link. After that, we analyze the influence of main system parameters on the OP and comparison between two cases with and without the presence of the direct link. Finally, the results show that all simulation and analytical results match well with each other based on the Monte Carlo verification simulation.

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1. INTRODUCTION

In the last decades, the Internet of Things (IoT) is a too hot research area over the world. With its potential to significantly influence all aspects of our daily lives, IoT is expected to have a significant impact on businesses by automating some processes and improving the control of many environment variables [1-6]. The wireless powered communication network (WPCN), where network devices harvest energy from the signals transmitted by RF energy sources in the first step and then utilize this harvested energy for their communication needs, is the primary direction in the RF energy harvesting. In the last decade, many research papers focused on WPCN and how to improve its efficiency. This concept of a tradeoff between EH and information transmission in WPCN was proposed and investigated in [7] and extended in [8]. Moreover, the concept of partial network level cooperation for EH networks was presented in detail in [9], and in [10] wireless EH and information transfer in cognitive relay networks was intensely analyzed. In WPCN, the two traditional time switching (TSP) and power splitting (PSP) protocols have been intensively studied in the literature, and many from these studies have compared the system performance of the two protocols under different scenarios [11-15].

In this work, we propose and investigate the outage probability (OP) of the Decode-and-Forward (DF) Energy Harvesting (EH) Full-Duplex (FD) Relaying network in Power Splitting Protocol (PS) using MRC Technique with the presence of the direct link. In the first stage, the integral form of the OP is derived in two cases with and without the presence of the direct link. After that, we analyze the influence of main system parameters on the OP and comparison between two cases with and without the presence of the direct link. Finally, the results show that all simulation and analytical results match well with each other based on the Monte Carlo verification simulation. The structure of this paper is proposed as follows. Sections II presents the system model of the relaying network. Sections III provides the analytical expression of OP in cases with and without the direct link between S and D. Section IV provides the numerical results and some discussions. Finally, Section V concludes the paper.

2. SYSTEM MODEL

Figure 1 plots the DF EH FD relaying network in the PS Protocol using MRC technique with the presence of the direct link. In this model system, the information is transferred from the source (S) to the destination (D), through energy constrained intermediate relay (R) and with the direct link. The energy harvesting and information processing of the system model with PS protocol are illustrated in Figure 2. In this scheme, T is the block time in which the source fully transmit the information data to the destination. In the first interval time (T/2), the relay harvests energy (ρ T) and transfers the information ((1- ρ)T) from the source signal to the destination, where ρ is the power splitting factor $\rho \in (0, 1)$. Here, we consider the interference noise at the relay node. In the remaining half-time T/2, the direct link transfers information from the source to the destination node. All the fading channels from S to R and R to D are proposed as the Raleigh fading channels [16-20].



Figure 1. System model



Figure 2. The power splitting protocol

3. THE SYSTEM PERFORMANCE

3.1. Energy Harvesting Phase

In the first time slot, the received signal at the relay can be expressed as

$$y_r = \sqrt{\rho P_s} h_{SR} x_s + n_r$$

(1)

Where x_s is the transmit signal at the source and where $E\{|x_s|^2\}=1$, $E\{\bullet\}$ is the expectation operator, Ps is transmitted power of the source, n_r is the additive white Gaussian noise (AWGN) at the relay R with zero-mean and variance N0.

The harvested energy at the relay can be given by

$$E_r = \eta \rho (T/2) P_s \left| h_{SR} \right|^2 \tag{2}$$

From (2), the average transmitted power at the relay can be obtained as

$$P_r = \frac{E_r}{T/2} = \eta \rho P_s \left| h_{SR} \right|^2 \tag{3}$$

Where $0 < \eta \le 1$ is the energy conversion efficiency and $0 < \rho < 1$ is the power splitting factor.

3.2. Information Transmission Phase

During the information transmission phase in the first time slot, the received signal at the relay can be given as [21-27]

$$y_r = \sqrt{(1-\rho)P_s}h_{sR}x_s + f\sqrt{P_r}x_r + n_r \tag{4}$$

Where x_r is the transmit signal at the source and $E\{|x_r|^2\}=1$, f is loopback interference channel. In the first time slot, the received signal at the destination in whole this time can be given as

$$y_d^1 = \sqrt{P_r} h_{RD} x_r + n_d^1 \tag{5}$$

Where n_d^i is the additive white Gaussian noise (AWGN) at the destination in the first time slot with zero-mean and variance N0.

In the second time slot, the destination will be received the signal directly from the source, which can be calculated as

$$y_d^2 = \sqrt{P_s h_{sD} x_s + n_d^2} \tag{6}$$

Where n_d^2 is the AWGN at the destination in the second time slot with zero-mean and variance N0. From (4), the signal to noise ratio (SNR) at the relay can be computed as the following

$$\gamma_{SR} = \frac{(1-\rho)P_s \left| h_{SR} \right|^2}{P_r \left| f \right|^2 + N_0}$$
(7)

Substituting (3) into (7) and using the fact that NO<<Ps, (7) can be rewritten as

$$\gamma_{SR} \approx \frac{(1-\rho)}{\eta \rho \left|f\right|^2} \tag{8}$$

From (5), the SNR at the destination in the first time slot can be calculated as the below equation:

$$\gamma_{RD} = \frac{P_r \left| h_{RD} \right|^2}{N_0} = \frac{\eta \rho P_s \left| h_{SR} \right|^2 \left| h_{RD} \right|^2}{N_0} = \psi \eta \rho \left| h_{SR} \right|^2 \left| h_{RD} \right|^2$$
(9)

$$\psi = \frac{P_s}{N_s}$$

Where we denote N_0 .

From (6), the SNR at the destination in the second time slot can be claimed as

$$\gamma_{SD} = \frac{P_s \left| h_{SD} \right|^2}{N_0} = \psi \left| h_{SD} \right|^2 \tag{10}$$

Using the MRC technique at the destination, the end to end SNR can be expressed as

$$\gamma_{e2e} = \begin{cases} \gamma_{RD} + \gamma_{SD}, & \text{if } \gamma_{SR} \ge \gamma_0 \\ \gamma_{SD}, & \text{if } \gamma_{SR} < \gamma_0 \end{cases}$$
(11)

Where $\gamma_0 = 2^{2R} - 1$ is the threshold of system and R is the target rate.

3.3. Outage Probability Analysis

$$OP = \Pr\left(\gamma_{SD} < \gamma_0, \gamma_{SR} < \gamma_0\right) + \Pr\left(\gamma_{SD} + \gamma_{RD} < \gamma_0, \gamma_{SR} \ge \gamma_0\right)$$

= $P_1 + P_2$ (12)

Where $P_1 = \Pr(\gamma_{SD} < \gamma_0, \gamma_{SR} < \gamma_0)$ and $P_2 = \Pr(\gamma_{SD} + \gamma_{RD} < \gamma_0, \gamma_{SR} \ge \gamma_0)$. Substituting (8) and (10) into P1, we have

$$P_{1} = \Pr\left[\frac{(1-\rho)}{\eta\rho|f|^{2}} < \gamma_{0}, \psi|h_{SD}|^{2} < \gamma_{0}\right] = \Pr\left[\frac{(1-\rho)}{\eta\rho|f|^{2}} < \gamma_{0}\right] \times \Pr\left(\psi|h_{SD}|^{2} < \gamma_{0}\right)$$
$$= \left\{1 - \Pr\left[|f|^{2} \le \frac{(1-\rho)}{\eta\rho\gamma_{0}}\right]\right\} \times \Pr\left(|h_{SD}|^{2} < \frac{\gamma_{0}}{\psi}\right)$$
$$= \left[1 - F_{|f|^{2}}\left(\frac{(1-\rho)}{\eta\rho\gamma_{0}}\right)\right] \times F_{|h_{SD}|^{2}}\left(\frac{\gamma_{0}}{\psi}\right) = \exp\left[\frac{\lambda_{f}(\rho-1)}{\eta\rho\gamma_{0}}\right] \times \left[1 - \exp\left(-\frac{\lambda_{SD}\gamma_{0}}{\psi}\right)\right]$$
(13)

Where $\lambda_{f}, \lambda_{SD}$ are the mean of the random variable (RV) $|f|^{2}$ and $|h_{SD}|^{2}$, respectively. Substituting (8), (9) and (10) into P2, we can obtain P2 as followings

$$P_{2} = \Pr\left(\psi \left|h_{SD}\right|^{2} + \psi \eta \rho \left|h_{SR}\right|^{2} \left|h_{RD}\right|^{2} < \gamma_{0}, \frac{(1-\rho)}{\eta \rho \left|f\right|^{2}} \ge \gamma_{0}\right)$$

$$= \Pr\left(\psi \left|h_{SD}\right|^{2} + \psi \eta \rho \left|h_{SR}\right|^{2} \left|h_{RD}\right|^{2} < \gamma_{0}\right) \times \Pr\left[\frac{(1-\rho)}{\eta \rho \left|f\right|^{2}} \ge \gamma_{0}\right]$$

$$= \left[1 - \exp\left(\frac{\lambda_{f}\left(\rho-1\right)}{\eta \rho \gamma_{0}}\right)\right] \times \Pr\left(\psi \left|h_{SD}\right|^{2} + \psi \eta \rho \left|h_{SR}\right|^{2} \left|h_{RD}\right|^{2} < \gamma_{0}\right)$$
(14)

Here, we consider

$$P_{3} = \Pr\left(\psi |h_{SD}|^{2} + \psi \eta \rho |h_{SR}|^{2} |h_{RD}|^{2} < \gamma_{0}\right) = \Pr\left(\psi \eta \rho |h_{SR}|^{2} |h_{RD}|^{2} < \gamma_{0} - \psi |h_{SD}|^{2}\right)$$
$$= \int_{0}^{\gamma_{0}} f_{X}(x) dx \int_{0}^{\gamma_{0}-x} f_{Y}(y) dy = \int_{0}^{\gamma_{0}} \left[F_{Y}(\gamma_{0}-x) - F_{Y}(0)\right] f_{X}(x) dx$$
(15)

Where we denote $X = \psi \eta \rho |h_{SR}|^2 |h_{RD}|^2$, $Y = \psi |h_{SD}|^2$ and

$$F_{Y}(y) = \Pr(Y < y) = \Pr(\psi |h_{SD}|^{2} < y) = 1 - \exp\left(-\frac{\lambda_{SD}y}{\psi}\right)$$

Easily to observe that $F_{\gamma}(0) = 0$. Hence, (15) can be rewritten as the following

$$P_{3} = \int_{0}^{10} F_{Y}(\gamma_{0} - x) f_{X}(x) dx$$
(16)

Continuing, we have to find $f_x(x)$ as the following steps

$$f_X(x) = \frac{\partial F_X(x)}{\partial x} \tag{17}$$

$$F_{X}(x) = \Pr\left(X < x\right) = \Pr\left(\psi\eta\rho \left|h_{SR}\right|^{2} \left|h_{RD}\right|^{2} < x\right) = \Pr\left(\left|h_{SR}\right|^{2} < \frac{x}{\psi\eta\rho \left|h_{RD}\right|^{2}}\right)$$
$$= \int_{0}^{\infty} F_{\left|h_{SR}\right|^{2}} \left[\frac{x}{\psi\eta\rho \left|h_{RD}\right|^{2}}\right] f_{\left|h_{RD}\right|^{2}} \left(\left|h_{RD}\right|^{2}\right) d\left(\left|h_{RD}\right|^{2}\right)$$
$$= 1 - \lambda_{RD} \int_{0}^{\infty} \exp\left(-\frac{\lambda_{SR}x}{\psi\eta\rho \left|h_{RD}\right|^{2}}\right) \times \exp\left(-\lambda_{RD} \left|h_{RD}\right|^{2}\right) d\left(\left|h_{RD}\right|^{2}\right)$$
(18)

Where λ_{SR} , λ_{RD} are the mean of the random variable (RV) $|h_{SR}|^2$ and $|h_{RD}|^2$, respectively. Apply (3.324,1) of the table of integrals in [28], (18) can be rewritten as the following

$$F_{X}(x) = 1 - 2\sqrt{\frac{\lambda_{SR}\lambda_{RD}x}{\psi\eta\rho}} \times K_{1}\left(2\sqrt{\frac{\lambda_{SR}\lambda_{RD}x}{\psi\eta\rho}}\right)$$
(19)

Where $K_{\nu}(\bullet)$ is the modified Bessel function of the second kind and vth order.

Substituting (19) into (17) and using the formulas
$$\frac{d}{dx} \left(x^{\nu} K_{\nu}(x) \right) = -x^{\nu} K_{\nu-1}(x)$$
, we have

$$f_{X}(x) = \frac{2\lambda_{SR}\lambda_{RD}}{\psi\eta\rho} \times K_{0} \left(2\sqrt{\frac{\lambda_{SR}\lambda_{RD}x}{\psi\eta\rho}}\right)$$
(20)

Substituting (20) into (16), we can claim P3 as following

$$P_{3} = \frac{2\lambda_{SR}\lambda_{RD}}{\psi\eta\rho} \int_{0}^{\gamma_{0}} \left[1 - \exp\left\{\frac{\lambda_{SD}\left(x - \gamma_{0}\right)}{\psi}\right\}\right] \times K_{0}\left(2\sqrt{\frac{\lambda_{SR}\lambda_{RD}x}{\psi\eta\rho}}\right) dx$$
(21)

Finally, substituting (21) into (14), we have

$$P_{2} = \frac{2\lambda_{SR}\lambda_{RD}}{\psi\eta\rho} \left[1 - \exp\left(\frac{\lambda_{f}(\rho - 1)}{\eta\rho\gamma_{0}}\right)\right] \times \left\langle \int_{0}^{\gamma_{0}} \left[1 - \exp\left\{\frac{\lambda_{SD}\left(x - \gamma_{0}\right)}{\psi}\right\}\right] \times K_{0}\left(2\sqrt{\frac{\lambda_{SR}\lambda_{RD}x}{\psi\eta\rho}}\right) dx \right\rangle$$
(22)

$$OP = \exp\left[\frac{\lambda_{f}\left(\rho-1\right)}{\eta\rho\gamma_{0}}\right] \times \left[1 - \exp\left(-\frac{\lambda_{SD}\gamma_{0}}{\psi}\right)\right] + \frac{2\lambda_{SR}\lambda_{RD}}{\psi\eta\rho}\left[1 - \exp\left(\frac{\lambda_{f}\left(\rho-1\right)}{\eta\rho\gamma_{0}}\right)\right] \\ \times \left\langle\int_{0}^{\gamma_{0}}\left[1 - \exp\left\{\frac{\lambda_{SD}\left(x-\gamma_{0}\right)}{\psi}\right\}\right] \times K_{0}\left(2\sqrt{\frac{\lambda_{SR}\lambda_{RD}x}{\psi\eta\rho}}\right)dx\right\rangle$$

$$(23)$$

4. NUMERICAL RESULTS AND DISCUSSION

In this section, we investigate the influence of energy coefficient η on the OP of the proposed system is plotted in Figure 1. In this paper, we set the main parameter as ψ =5 dB, ρ =0.5, R=0.5 and 1. From the results, we can see that the OP has a slight decrease while η increases from 0 to 1. Besides, the OP of the proposed system in the case with the direct link between the S and D is better than in the case without the direct link. Moreover, the OP versus ψ is illustrated in Figure 4 with the main parameters as η =0.8, ρ = 0.25 and 0.85. The results show that the OP decreases with the rising of ψ . However, the OP in the case without the direct link between the S and D has a considerable decrease in comparison with the OP in the case without the direct link. In all above Figures., all the simulation and analytical results are the same with both cases with and without a direct link between S and D.

Furthermore, the effect of R and ρ on the OP of the proposed system are drawn in Figures 5 and 6. We set some main parameters of the system as $\psi = 5$ dB, $\rho = 0.5$, $\eta = 0.8$. Figure 5 shows that the Op increases crucially when R rises from 1 to 2 then has the same value as R from 2 to 7. The OP has a slight decrease the increases when ρ varies from 0 to 1. From the above Figures., we can see that the OP in the case without direct link is better than in the case with the direct link. All the simulation result agree well with the analytical results as shown in Figures 5 and 6. OP versus η as shown in Figure 3.



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5. CONCLUSION

In this paper, we propose and investigate the OP of the DF EH FD relaying network in the PS Protocol using MRC technique with the presence of the direct link. In the first stage, the integral form of the OP is derived in two cases with and without the presence of the direct link. After that, we analyze the influence of main system parameters on the OP and comparison between two cases with and without the presence of the direct link. Finally, the results show that all simulation and analytical results match well with each other based on the Monte Carlo verification simulation. The research results can be proposed as a recommendation for manufacturing EH relaying communication network.

ACKNOWLEDGEMENTS

This research was supported by National Key Laboratory of Digital Control and System Engineering (DCSELAB), HCMUT, VNU-HCM.

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