

Javanese Gong Acoustics and Its Modeling using Finite Element Method

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Abstract

In Central Java, the Javanese Gong is one of prominent gamelan instrument to mark the end of musical passage. The Gong is a distinctive percussion instrument because of its wave-like sounds after being struck immediately due to its traditional manufacture procedures. Spectra for the gongs vary substantially due to variation in shape and size, and to dimensional irregularities created during manufacture and whilst tuning by soft-hammering or hand-grinding. Finite Element Analysis is used to predict the effect of a range of variations of gong geometries on modal shapes as well as modal frequencies. The radiated sound spectra of the gong are also measured and compared with the natural frequencies obtained from Finite Element Analysis. Through the finite element model, the effect of geometric dimensions and material properties of the gong on its sound characteristics can be predicted.

Keywords: Javanese gong, modal frequencies, mode shapes, finite element method, acoustic spectra

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1. Introduction

The Javanese Gong plays an important role in Javanese culture. In gamelan music ensemble, gong sound marks and ends certain passage of a gamelan composition [1]. The gong sound is also used to declare the opening and closing of important either religious and secular events or various rituals. The roaring wavelike sound of the gong is associated by Javanese with Bima's giggle that creates a grandeur yet calming feeling. Bima is known as a courageous but honest and just hero, a great legend in Javanese puppet shadow (wayang) stories. The number of wavelike sound repetition cycles in a best sounding gong can be as many as 12 to 13. A Gong is still traditionally handmade by casting, hammering, forging and tuning as well. In this research we studied the 56 cm diameter of iron Gong Kempul, a second largest gong in the complete set of Javanese Gamelan instrument. Although an iron gong is less expensive kind of gong that is mainly used for educational purposes, it is still crafted to produce the wavelike sound. The gong was tuned to tone 6 in *pelog* scale [1, 2].

Gamelan instruments makers usually make most of the metal based instruments based on their experiences and intuitions. There are few studies investigating their vibration and sound characteristics. Tsai et al. [3] constructed finite element model of a Chinese copper gong and obtained the natural frequencies and corresponding mode shapes. Then, experimental modal analysis was carried out to compare with the findings obtained from finite element model. The sound spectra were measured to identify to fundamental frequency. Finite element analysis has been widely used to model complex shapes. Yusoff et al. [4] highlighted the detail descriptions that lead to five-phase supply with fixed voltage and frequency by using Finite-Element Method (FEM). Identifying of specification on a real transformer had been done before applied into software modeling. Therefore, Finite-Element Method provides clearly understandable in terms of visualize the geometry modeling, connection scheme and output waveform. George et al. [5] presented finite element modeling and results of a five-phase permanent magnet brushless motor designed for high power density application, exploring the characteristics of multiphase topology. Bretos et al. [6] adopted finite element method to model the free plates and box of violin, excepting the neck. Through the validated finite element model, the adjustment of violin modal properties can be numerically predicted and fitted to desired resonance peaks. Maclachlan [7] employed Finite Element Analysis to predict the effect of a range of variations of gong geometries on modal frequencies. The predicted frequencies of the Finite Element

Analysis experiment for gong models did not match the acoustic spectra for these gongs. Lu [8] presented a study of the vibrational behaviour of the violin top plate and explored the possibility of using composite materials as a substitute for traditional wood in making top plates. Numerical simulations and experimental tests are compared to validate the results. The two most popular methods for numerical and experimental vibrational analysis, the Finite Element Method (FEM) and Experimental Modal Analysis are used, respectively. Then, the same modeling and testing techniques were applied on two composite plates. Results show that the vibrational behavior of composite plates differs significantly from traditional wooden plates. Facchinetti et al. [9] applied finite element analysis (FEA) and experimental mode analysis (EMA) to study the vibration behaviors of reed and pipe in clarinet. The holographic interferometer was used to observe the vibration modes and eigen-frequencies of the reed. The experimental results showed that some reeds had strong asymmetries; the cause of modal asymmetries lies most probably in the lack of homogeneity of the cane used for the reed due to its natural character. To understand the vibration behavior of musical instruments and their sound mechanism, experimental techniques are necessary. Wang [10] presented the approach of virtual testing (VT) by the integration of finite element analysis (FEA) and experimental modal analysis (EMA) techniques for the design analysis of several types of percussion instruments. First, the procedure for model verification is introduced and shown the basic principle for validating the finite element model by adopting FEA software and performing EMA. The sound spectrum of percussion instrument can then be measured to identify the most contributed structural modes and compared with those modal parameters obtained from FEA and EMA. Three types of percussion instruments, including a xylophone bar, a metallophone plate and a gong, are shown to demonstrate the idea of VT for the redesign of new type of percussion instruments. Skrodzka and Sek [11] adopted the traditional experimental modal analysis techniques to get modal frequencies, modal damping ratios, and their corresponding mode shapes of a loudspeaker under different working conditions. The vibration frequencies and the mode shapes for a semi-cone woofer and a tweeter were observed. Finite element analysis modeling has been applied to the design of novel idiophones for use within conventional European musical contexts [12]. Computer programs which physically model musical instruments through FEA modeling have recently been developed for electronic music synthesis [13]. This work adopts FEA to study the vibration characteristics of an iron Gong Kempul. It is made of malleable cast iron, with material properties as follow: elastic modulus of 1.9×10^{11} Pa, poisson's ratio of 0.31, mass density of 7200 kg/m^3 , tensile strength of 861×10^6 Pa, and yield strength of 827×10^6 Pa. Figure 1 shows the design of the gong and its dimensions. The sound frequency response is also measured to find the relationship between the dynamic modes and sound qualities. From the FEA model, the effect of geometry dimensions and material properties on the principal frequency is also observed.

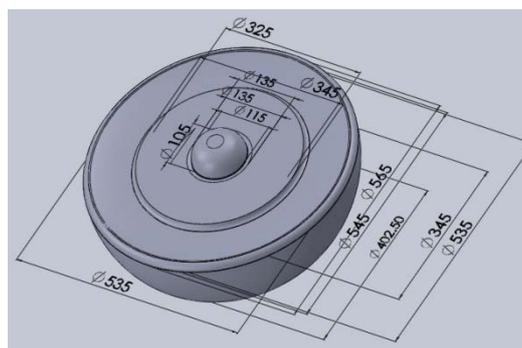


Figure 1. Dimension of gong kempul in millimeters

2. Finite Element Analysis in Solidworks

The SolidWorks is an engineering 3D CAD software for Microsoft Windows. It has three degrees of function for the needs of organizations. The SolidWorks Standard is suitable for fast modeling; design in 2D and in 3D. The SolidWorks Professional is the superstructure of SolidWorks Standard. It improves the efficiency and innovates with solutions that are used by

millions of designers. It contains additional extension modules as Animator, PhotoWorks, etc. The SolidWorks Premium is the most comprehensive software. It combines the capabilities of the SolidWorks Professional with simulations. The Part of the SolidWorks Professional is the SolidWorks Simulation, which provides basic simulation tools for testing stress, strain, analyzing the kinematics, dynamics and its simulation conditions of the real world [14].

2.1. Boundary Condition

The material properties are assigned to the gong and boundary conditions are determined. The gong's all degrees of freedom on surface are taken. They are denoted with the green flag in Figure 2. These two holes are fixtures through which hanging ropes hold the gong. This condition prevents the movement of the surface in a space.



Figure 2. Boundary conditions

2.2. Mesh Configuration

Mesh on the gong is generated automatically by SolidWorks. The element is defined by 10 nodes while each node has three degrees of freedom at each node. The spatial element has 16 Jacobian points and is suitable for modeling of the finite element irregular mesh. The maximum size of the element is 33.8607 mm with tolerance of 1.69 mm. The mesh in Figure 3 is created of 8523 elements and of 17026 nodes.

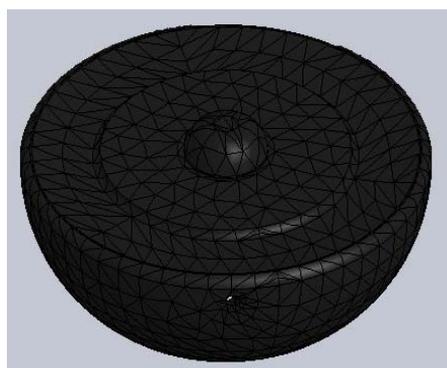


Figure 3. Mesh of finite element of gong

2.3. Modal Analysis of Gong

The modal analysis is carried out by SolidWorks and mode shapes and natural frequencies are also calculated. For this modal analysis the direct solver including the FFEPlus method is used. The first five mode shapes are shown in Figure 4, and the first five natural frequencies are shown in Table 1.

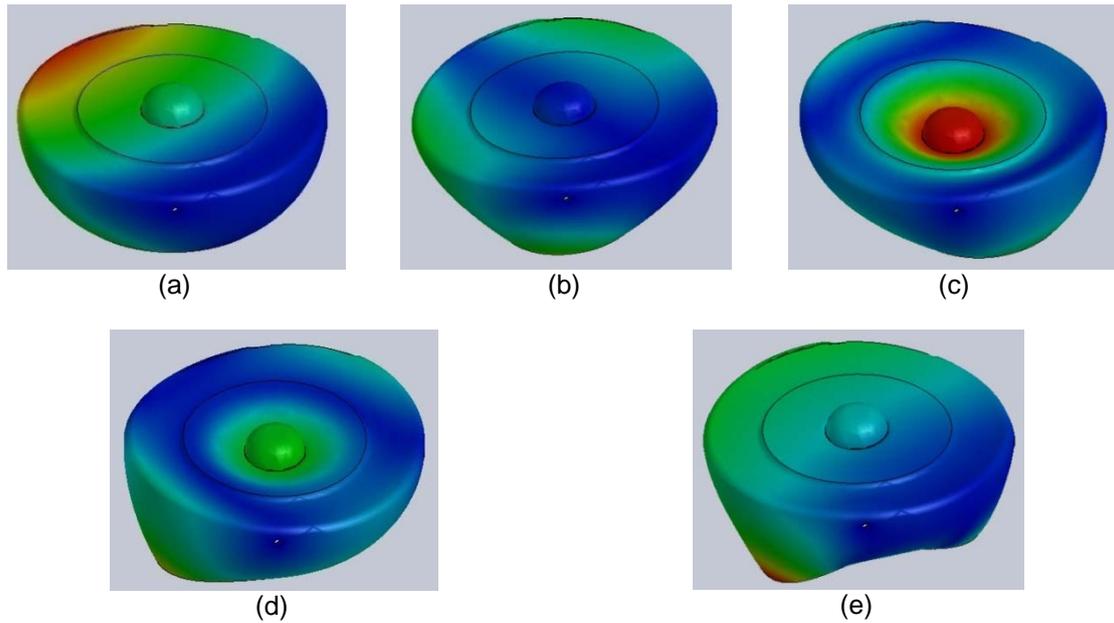


Figure 4. Mode shapes of gong: (a) First Mode (b) Second Mode (c) Third Mode (d) Fourth Mode (e) Fifth Mode

Table 1. Natural Frequencies of Particular Mode Shapes

Mode shape	1	2	3	4	5
Frequency (Hz)	78.506	224.74	344.2	397.84	533.53

3. Acoustics Spectra of the Gong

We recorded 48kHz sample tones of the Gong Kempul using ARTA PC Software. A controlled gong striker was utilized to exert a controlled impact force upon the gong boss, as seen in Figure 5. First, a measurement condenser microphone acquired the acoustic signal by near field measurement from behind of the boss, externally powered by a phantom power. A sound card then interfaced and digitized this signal in order that computers are able to recognize.



Figure 5. Measurement setup

An impulse-generated response was recorded to analyze in both the time and frequency domain as shown in Figure 6. The spectral peaks indicate partials with significant strength. Table 2 shows the 18 consistent partials, averaged from four trials, of the gong consisting of both harmonis and nonharmonic frequencies [15]. The partials at 93.02 Hz, 186 Hz,

279.1, 372.1, and 464.9 Hz are the strict integer multiples of the fundamental frequency. Hence, these partials are the first, second, third, fourth, and fifth harmonics, respectively. Such degree of harmonicity of the partials leads to the pitched sound of the Gong Kempul, differing it from that of Chinese gongs which sound like a crash. The harmonic and or inharmonic partials that occur in fairly close frequency beat together and form the roaring sound which is often associated with Bima's laughter [16-17].

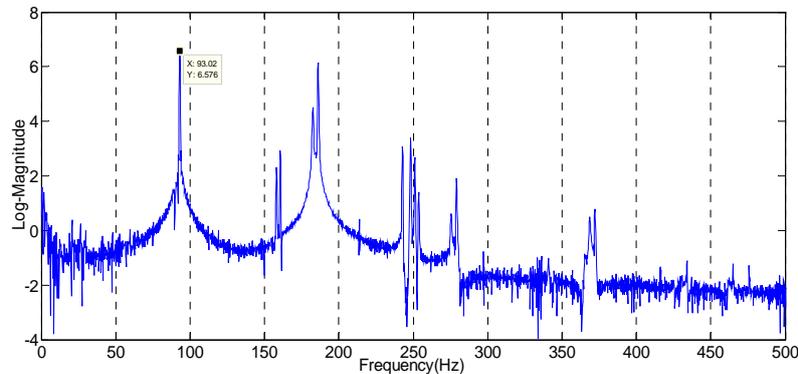


Figure 6. Acoustics spectra of the gong

Table 2. Partial of the Spectra

No	Partials (Hz)	Harmonics
1	93.02	1 st
2	158.2	
3	160.5	
4	182.7	
5	186	2 nd
6	213.9	
7	242.9	
8	248.2	
9	251.6	
10	253.4	
11	275.8	
12	279.1	3 rd
13	368.9	
14	372.1	4 th
15	433.9	
16	462.3	
17	464.9	5 th
18	475.7	

Table 3. Differences between predicted and measured natural frequencies (Hz)

Mode	1	2	3	4	5
FEA	78.506	224.74	344.2	397.84	533.53
Spectra	93.02	186	279.1	372.1	464.9
Absolute Error (%)	15.6	20.82	23.32	6,91	14.7

As shown in Table 3, the predicted frequencies of the finite element analysis experiments for gong model based on manufactured gongs did not match the acoustics spectra for these gongs due to various effects of the manufacturing processes which are difficult to accurately model. The gong makers are used to mix the raw material, composed by tin and copper, with a certain ratio. Besides, they fine-tune the gong using soft hammer by tapping the outer part of boss, therefore, there are many irregularities from one gong to another gong.

For more understanding of the geometric dimensions and material properties' effects on the sound characteristics of the gong, finite element models are created with different properties. Table 4 lists natural frequencies for different cases. The first modification doubles

the thickness from 5 mm to 10 mm, whereas, the second modification change the gong material to copper-tin alloy with elastic modulus of 1.1×10^{11} Pa, Poisson's ratio of 0.33, and mass density of 8300 kg/m^3 .

Table 4. Natural frequencies (Hz) for different properties

Mode	Original case	Double size of thickness	Original size (copper alloy)
1	78.506	85.661	52.494
2	224.74	305.93	150.19
3	344.2	334.13	219.04
4	397.84	462.25	259.91
5	533.53	476.56	348.96

It is obvious that increasing the size dimensions will generally lower the fundamental frequencies as that found in gamelan set for both *pelog* and *slendro* scale. However, increasing the thickness of the gong will result in higher natural frequencies. For lower stiffness material, the natural frequencies are lower than those of for higher stiffness material.

4. Conclusion

In this study, the finite element model of a Javanese gong is constructed. The sound characteristics of the copper gong are also investigated. The result obtained from finite element analysis show much difference since there are many concavities and convexities on the surface of the gong resulting from traditional manufacturing especially during fine-tuning process. In finite element analysis, structural dimensions and material properties of the gong can be changed to better understand the effect in vibration behavior and sound characteristics. Through these analyses, the gong structure can be modified to improve its sound characteristics. In future, an experimental modal analysis needs to be carried out to verify the model generated using finite element method.

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