Network loss reduction and voltage improvement by optimal placement and sizing of distributed generators with active and reactive power injection using fine-tuned PSO

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ABSTRACT

Minimization of real power loss and improvement of voltage authenticity of the network are amongst the key issues confronting power systems owing to the heavy demand development problem, contingency of transmission and distribution lines and the financial costs. The distributed generators (DG) has become one of the strongest mitigating strategies for the network power loss and to optimize voltage reliability over integration of capacitor banks and network reconfiguration. This paper introduces an approach for the optimizing the placement and sizes of different types of DGs in radial distribution systems using a fine-tuned particle swarm optimization (PSO). The suggested approach is evaluated on IEEE 33, IEEE 69 and a real network in Malaysian context. Simulation results demonstrate the productiveness of active and reactive power injection into the electric power system and the comparison depicts that the suggested fine-tuned PSO methodology could accomplish a significant reduction in network power loss than the other research works.

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1. INTRODUCTION

In today's world, the electrical power systems are confronting various technical issues, as consequences to the increased load growth of the last mile networks. These issues will further lead the networks to larger power losses, voltage drops, load imbalances and stability problems. Therefore, DGs have come up as a viable way of relieving such issues in a radial distribution network [1]. In [2], the DGs are defined as power generating sources, which are connected to the distribution systems, having a typical capacity of less than 50-100 MW. Small generators supplying the electric power required by the customers and these are scattered in a power system, is another definition of DGs [3, 4].

DG units generate power closer to the load centers, thus avoid the cost of energy transportation and reduce the power losses in transmission lines. Furthermore, the cost savings of the DG technologies are higher compared to the centralized generation station [5]. Normally, DGs are smaller in size and could be operated in stand-alone mode or in correlation with distribution network [6]. Hence, their impact on power system operation, control and stability depend on the DG size and the integrating location [7, 8]. However, non-optimized placement and sizing might increase the power losses as well as the violations in voltage statutory limits. Based on power injections, DGs have been classified in to four sections. Type I DGs only

inject active power and type II DGs inject both active and reactive power. Type III DGs inject only reactive power, while type IV DGs inject active power and absorb reactive power.

At present, it has become very clear that the reactive power support is an essential requirement for the well-executed distribution networks. Integration of capacitors has been often used to compensate reactive power. Therefore, improvement in voltage profile within the acceptable limits minimizes power and energy losses. Many researchers have studied on optimal capacitor placement using different methods [9, 12]. However, the ability of injecting both active power and reactive power of DGs enhance the system performance than that of injecting only reactive power by power loss reduction.

In recent research work, many approaches have been undertaken to obtain a minimum network power loss by integration of DGs. These approaches can be mainly categorized as classical and artificial Intelligent algorithms [13]. A comparative study for DG allocation techniques based on active power and reactive power indices and voltage loss reduction has been addressed in [14]. In [15], a nonlinear programming (NLP) multi objective framework has been proposed for the perfect sitting and sizing of DG units. Minimizing the number of DGs and power losses together with maximizing the voltage stability margin are the objectives of this approach. An improved analytical method has been presented in [16] focusing on the identification of the best location of integration. But most of the analytical methods have been antiquated due to more time consumption and the less accuracy.

Genetic algorithms [17], Harmony search [18], particle swarm optimization (PSO) [19-21], and Tabu search [22] are some of the artificial intelligence techniques, that have been used to determine the optimal location and the size of the distributed generators. The main feature of the popularity of these techniques is the computational robustness. Reference [23] has presented a DG placement and sizing method considering reduction of system losses, voltage magnitude and stability enhancement. In [24], a new robust power flow method with whale optimization has been proposed for DG placement and sizing. Most of the research work related to optimal placement and sizing of DGs using PSO techniques disclose a low percentage of loss reduction. The usage of un-tuned PSO parameters is the principal cause for that poor loss reduction. Parameter selection could be identified as the key influence of the productivity and the performance.

In this paper, a fine-tuned particle swarm optimization approach and voltage stability index (VSI) have been used to determine the optimal size and location of the DGs to minimize the power losses while maintaining the voltage profile and stability margin. The algorithm parameters of PSO have been selected to obtain the minimum loss reduction. Most of the approaches presented so far have been utilized only type I DGs to the network to determine the optimal size and the location. In the current work, the capability of improving the power loss reduction and the voltage stability have been investigated by integrating both type I and type II DGs to the network systems. The effectiveness of the proposed approach is demonstrated on standard IEEE 33 bus, IEEE 69 bus and a real Malaysia 54 bus network system. The integration of type II DGs is suggested to improve the reduction of power loss and the voltage stability of the system.

2. RESEARCH METHOD

2.1. Problem formulation

2.1.1. Objective function

The main objective of allocating DGs in a distribution network is to get the maximum feasible benefits by enhancing the system's efficiency in terms of improving the power loss reduction. The problem could be mathematically formulated as an objective of minimizing the loss of real power.

Minimize
$$P_L = \sum_{i=1}^{N} P_{loss} = \sum_{i=1}^{N} I_{br,i}^2 \times R_i \text{ for } i = 1, 2 \dots N$$
 (1)

where $I_{br,i}$, R_i and N are the i^{th} branch current, the i^{th} branch resistance and number of branches respectively.

2.1.2. Constraints

a) Voltage Constraints

Absolute value of the voltage magnitude at each node must be stationed within their allowable ranges in order to maintain the system's power quality. It is defined as below.

$$|V_{min}| \le V_i \le |V_{max}| \text{ for } i = 1, 2 \dots M$$
⁽²⁾

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b) DG capacity constraints

Total connected DG units' active and reactive power generation must be lower than the base system's active and reactive power loads. Furthermore, it should be lower than the DG's maximum generation capability. Mathematically, this constraint was defined as follows:

$$P_{DG,min} < P_{DG} < P_{DG,max} \tag{3}$$

$$Q_{DG,min} < Q_{DG} < Q_{DG,max} \tag{4}$$

Assuming,, $\alpha = tan(cos^{-1}(PF))$, where *PF* is the power factor of DG unit, the generated reactive power can be expressed as:

$$Q_{DG} < \alpha P_{DG} \tag{5}$$

For type I DGs, $\alpha = 0$ and for type II DGs, $0 < \alpha < 1$. The injected reactive power Q_i at i^{th} bus is:

$$Q_i = \alpha P_{DG} - Q_d \tag{6}$$

where Q_i is the net reactive power demand at i^{th} bus. The thermal limit must not exceed its limits.

$$S_i \leq S_{max} \text{ for } i = 1, 2 \dots N \tag{7}$$

2.2. Particle swarm optimization (PSO)

PSO algorithm is one of the evolutionary computation techniques that optimizes an objective function by iteratively attempting to improve a solution by giving considerations to predefined measure of quality. In this research work, PSO algorithm has been used to establish the optimal size of the DGs. An outline of the PSO with steps is given below. PSO algorithm is a population-based search algorithm oriented on the simulation of the social behavior of a birds' flock, introduced originally by Kennedy and Eberhart in 1995 [25]. The n number of particles in the swarm represent the nominee solutions. Each particle is a real valued m dimensional vector where m is the number of parameters optimized. Consequently, every optimized parameter represents a dimension of the problem space.

- **Step 1:** Insert the data of the network for the power flow simulations and initialize parameters of PSO algorithm (i.e. number of iterations, number of particles, social coefficient (C_2), cognitive coefficient (C_1), minimum and maximum limits of inertia weight)
- Step 2: Construct randomly initialized swarm matrices for the position and velocity and run the base case power flow.
- Step 3: Use forward and backward sweep method to power flow simulations and compute the loss of active power (fitness function) using (1), the nodal voltages, and the flow of power in each line.
- Step 4: Test on the network constraints comprising the voltages of the nodes, DG capacity and line power flows which is the thermal capacity as shown in (2) to (4) and (7). If all the constraints are satisfied, proceed to step 6; otherwise proceed to the next step.
- Step 5: Employ the penalty function method (PFM) for the DGs which are in breach of the constraints.
- Step 6: Identify the best personal experience (*Pbest*) of each particle and the best global experience (*Gbest*), out of every particle in the swarm.
- Step 7: Update each particle's position (x_{id}^{k}) and velocity (v_{id}^{k}) using (9) and (10). ω is the inertia constant and *rand*() is a randomly generated number $\in [0 \ 1]$. The equation for linearly increasing inertia constant in each iteration is shown in (8).

$$\omega = \frac{(\omega_{max} - \omega_{min})}{it_{max}} \times it \tag{8}$$

$$v_{id}^{k+1} = \omega v_{id}^{k} + C_1 rand() \times (P_{best} - x_{id}^{k}) + C_2 rand() \times (G_{best} - x_{id}^{k})$$
(9)

$$x_{id}^{k+1} = x_{id}^{k} + v_{id}^{k+1} \tag{10}$$

2.3. Voltage stability index

The placement of the DGs is conducted by randomly choosing the positions from the VSI node array. The VSI node array is composed of the nodes, which have an index less than 0.9 as the nodes with

lower values are more sensitive to collapse. The VSI is formed utilizing transferred active power and reactive power in a line as in (11).

$$VSI = 2|V_r|^2|V_s|^2 - |V_r|^4 - 2|V_r|^2\{P_iR_i + Q_iX_i\} - |z_i|^2\{P_i^2 + Q_i^2\}$$
(11)

where, V_r , V_s , P_i , Q_i , R_i , X_i and $|z_i|$ are receiving end voltage, sending end voltage, active power of the load at i^{th} bus, reactive power of the load at i^{th} bus, resistive component of the i^{th} line, reactive component of the i^{th} line and impedance of the i^{th} line respectively.

2.4. Methodology

The fine-tuned PSO technique for standard IEEE 33 bus, IEEE 69 bus and a real Malaysia 54 bus networks were implemented and simulated on MATLABTM simulation platform. The Malaysia 54 bus network is shown in Figure 1. Initially, Type I DGs were integrated and increased up to three number of DGs and recorded the results. Then Type II DGs with a PF of 0.9 were integrated to all the networks and followed the same procedure. The perfect solution for the placement and sizing in every network were obtained by performing PSO algorithm with the population size of 30.

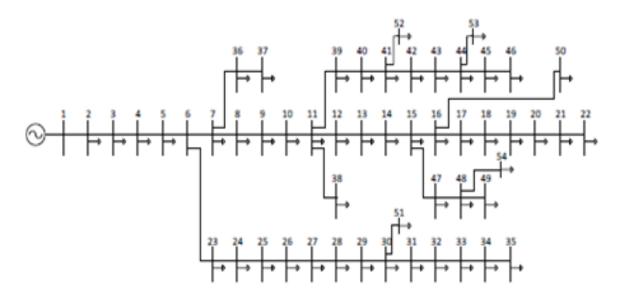


Figure 1. Malaysia 54 bus network

3. RESULTS AND DISCUSSION

The implemented routines described under methodology section were simulated and the optimal locations and sizes of DGs, voltage profiles, real power loss data were obtained. Figure 2(a), Figure 2(c) and Figure 2(e) present the voltage profiles after type I DG integration for IEEE 33 bus, IEEE 69 bus and Malaysia 54 bus networks respectively considering the unity power factor DGs. Figure 2(b), Figure 2(d) and Figure 2(f) depict the voltage profiles after type II DG integration for IEEE 33 bus, IEEE 69 bus and Malaysia 54 bus networks respectively and the power factor of every DG is defined as 0.9. In each graph under Figure 2, the base case without DGs, one DG, two DGs and three DGs were represented by blue, green, red and pink colour lines respectively. The statutory voltage limits of 1.05 pu (upper limit–red) and 0.95 pu (lower limit-purple) were marked in dashed lines for clear illustration of the voltage profile. Figure 3 shows the active and reactive power losses for every network described under methodology section. In addition, convergence of the PSO algorithm is also acquired for the accuracy of the algorithm. Figure 4 shows the voltage profiles of three DG integrations, obtained for every type of DGs. 0.9 lagging and 0.9 leading power factors are used for type II and type IV DGs respectively. The results for optimal siting and sizing, power loss and power loss reduction percentage for each network were described in Table 1.

3.1. IEEE 33 bus system

With a total load of 3.72 MW and 2.30 Mvar, the IEEE 33 bus system is a radial distribution network. The overall active power loss in the base case system is 210.07 kW, whereas total reactive power loss is 142.337 kvar. By examining the Figure 2(a), it was observed that, the base system has violated the lower statutory voltage limit at two intervals of the network. The voltage profiles after adding one, two and three DGs with unity PF show a growth in nodal voltage levels of base system and they lie inside the allowable boundaries except in one DG scenario. The single DG placement has yielded a network power loss reduction of 51.37%, and it has increased to 65.29% after the placement of three DGs. However, the DGs with 0.9 PF have reinforced the all voltage profiles higher than the lower statutory limit and there is an improvement in voltage profile compared to the DG integration with a unity power factor. It could be seen as shown in Figure 2(b). The maximum power loss reduction achieved by three DGs, having a 0.9 PF is 89.54% and it was 68.09% for single DG and 83.69% for two DGs. The DG sizes were varied from 0.7 MVA to 3 MVA for both type of DGs.

3.2. IEEE 69 bus system

The IEEE 69 bus system has connected to a total active load of 3.791 MW and a reactive load of 2.694 Mvar. The active power loss and the reactive power loss without integrating DGs are 238.14 kW and 106.76 kvar respectively. By reviewing Figure 2(c), the single DG with unity PF has contributed a loss reduction of 65.35%. Similarly, 69.07% and 69.72% are the loss reductions achieved by two and three DGs respectively. As shown Figure 2(d), it was revealed that a considerable voltage improvement for the segment after 50th bus was achieved by injecting reactive power in one, two and three DG scenarios. The power loss reduction for single DG with 0.9 PF is 88.50% and 94.01% for two DGs with the same PF. Maximum loss reduction percentage was recorded with type II three DGs and it is 94.95%. The optimal DG sizes were varied from 0.5 MVA to 4 MVA for both type of DGs.

3.3. Malaysia 54 bus system

The Malaysia 54 bus system is also a radial distribution network with a total active load of 4.595 MW and reactive load of 2.298 Mvar. The active and reactive power losses are 338.46 kW and 242.28 kvar respectively. The system has violated the lower voltage limit in three sections. As expected, the violated voltage nodes have risen up their voltage magnitude by injecting type I DGs to the network system. It has achieved 72.26% from one DG, 78.0% from two DGs and 79.64% from three DGs. The improved variations in nodal voltages compared to the base system could be seen in Figure 2(e).

The Figure 2(f) shows how the nodal voltages in Malaysia network are deviated using both active and reactive power. It has significantly improved than that of injecting only active power and could be clearly observed from the graphs. The loss reduction has advanced up to 86.53% by adding single DG with 0.9 PF and it was an increment in performance than three DGs with unity PF. After placing of DGs at perfect locations and sizes given by PSO algorithm, the network has attained a maximum power loss reduction of 96.25% by type II DGs. The active and reactive power losses in all the networks are shown in Figure 3. As presumed, it demonstrates the reduction of power losses with the number of DGs connected as well as the type of the DG. Type II DGs (with 0.9 PF) have exhibited the maximum power loss reduction.

Figure 4 shows the gained loss reduction of type II DGs compared to the type I DGs and it has increased between 15% and 25%. The variation of nodal voltages in IEEE 33 bus network for every type of DGs were shown in Figure 5. The least growth in voltage could be seen by type III DGs, which injects only reactive power. The next enhancement in nodal voltage was indicated by type IV DGs and it injects active power and absorbs reactive power. A moderate increment compared to the base system was displayed by type I DGs. They only inject active power. Type II DGs have achieved the best gain in nodal voltages by injecting both active and reactive power to the base system. Number of DGs were retained at three for all the cases described in Figure 5 and the leading and lagging PFs were fixed at 0.9. Table 2 shows the comparison of the results with other studies undertaken with unity PF and 0.866 lagging PF for IEEE 33 bus system. It is observed that the total loss reduction in proposed fine-tuned PSO technique is higher than the other methods. The percentage reduction in total losses are 65.29% and 92.09% for the DG penetrations with unity PF and 0.866 lagging PF respectively.

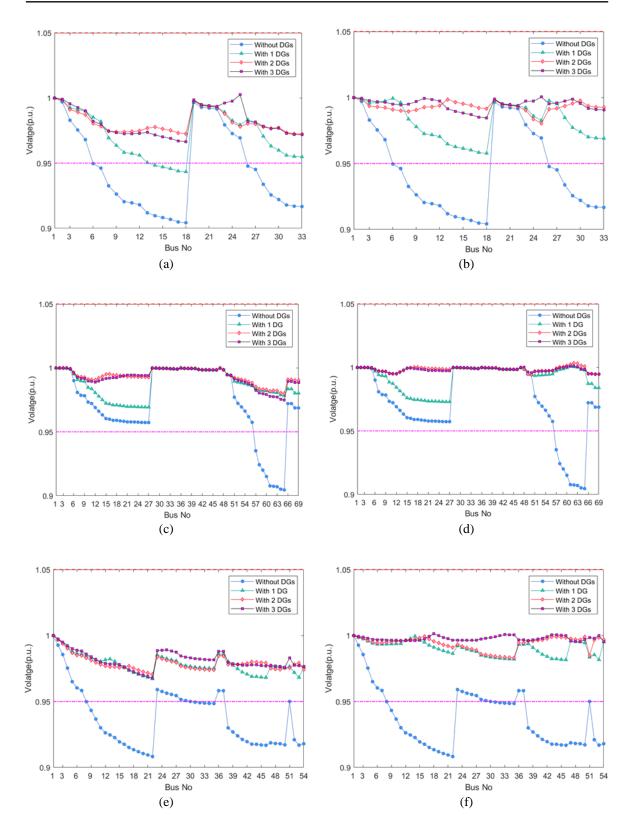


Figure 2. Variation of voltage profiles, (a) IEEE 33 bus (type I DG), (b) IEEE 33 bus (type II DG), (c) IEEE 69 bus (type I DG), (d) IEEE 69 bus (type II DG), (e) Malaysia 54 bus (type I DG), (f) Malaysia 54 bus (type II DG)

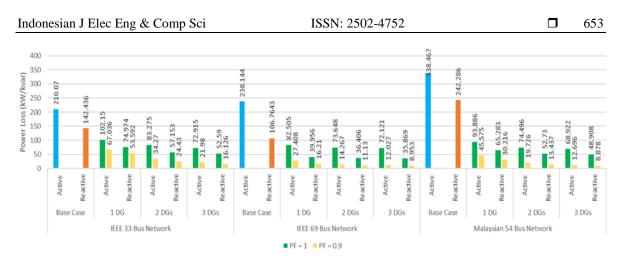


Figure 3. Active and reactive power losses of all networks

	Domon	1 st	1 st DG	2 nd	2 nd DG	3 rd	3 rd DG	Activo	Depative	Loca
Network	Power	-						Active	Reactive	Loss
	Factor	DG	Size	DG	Size	DG	Size	Power	Power	Reduction
	(PF)	Node	(MW)	Node	(MW)	Node	(MW)	Loss(kW)	Loss(kVar)	(%)
IEEE 33 Bus System	Base	-	-	-	-	-	-	210.070	143.437	-
		6	2.659	-	-	-	-	102.150	74.974	51.37
	1	30	1.243	12	0.815	-	-	83.275	57.153	60.36
		16	0.700	25	1.492	30	1.158	72.915	52.590	65.29
		6	2.920	-	-	-	-	67.036	53.592	68.09
	0.9	13	0.913	30	1.464	-	-	34.270	24.430	83.69
		29	1.272	25	0.833	10	0.894	21.980	16.126	89.54
	Base	-	-	-	-	-	-	238.144	106.464	-
IEEE 69 Bus System		61	1.999	-	-	-	-	82.505	39.956	65.35
	1	62	1.909	16	0.710	-	-	73.648	36.406	69.07
		3	3.941	61	1.878	21	0.556	72.121	35.869	69.72
		61	2.192	-	-	-	-	27.408	16.210	88.50
	0.9	17	0.622	62	2.133	-	-	14.267	11.130	94.01
		61	1.895	16	0.567	48	1.288	12.027	8.953	94.95
Malaysia 54 Bus System	Base	-	-	-	-	-	-	338.467	242.286	-
		14	4.074	-	-	-	-	93.886	65.283	72.26
	1	43	1.885	17	2.138	-	-	74.496	52.738	78.00
		15	2.330	25	1.010	43	1.329	68.922	48.908	79.64
		14	4.099	-	-	-	-	45.575	30.216	86.53
	0.9	44	1.590	16	2.653	-	-	19.726	13.437	94.17
		18	2.001	33	0.556	43	1.554	12.696	8.878	96.25

Table 1. Simulation results for test networks

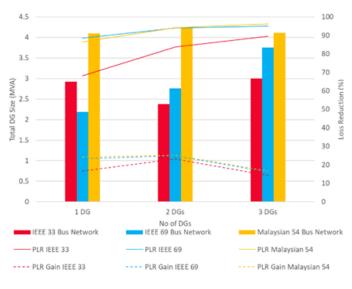


Figure 4. DG sizes and increment in loss reduction

Network loss reduction and voltage improvement by optimal placement and sizing of.. (Eshan Karunarathne)

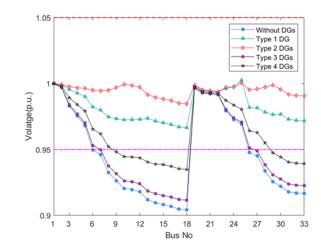


Figure 5. Voltage profiles of all types of DGs for IEEE 33 bus network

Table 2. Comparison of simulation results of IEEE 33 bus system with other research works

Ref.	Method	Р	ower factor =1		Power factor =0.866			
Kei.	Wiethiou	Location	Size(MVA)	LR(%)	Location	Size(MVA)	LR(%)	
Proposed PSO Algorithm		16	0.7000		25	0.7965	92.09	
		25	1.4922	65.29	30	1.3646		
		30	1.1589		13	0.7382		
[26]		11	1.5000		-	-	-	
	GA	29	0.4228	49.61				
		30	1.0714					
[26]		13	0.9816		-	-	-	
	PSO	32	0.8297	50.06				
		8	1.1768					
[26]		32	1.2000		-	-	-	
	GA/PSO	16	0.8630	50.99				
		11	0.9250					
[27]		6	1.1124		6	1.1976	87.33	
	SA	18	0.4874	61.12	8	0.4778		
		30	0.8679		10	0.9205		
[28]		14	0.6521		14	0.6798	82.06	
	BFOA	18	0.1984	57.38	18	0.1302		
		32	1.0672		32	1.1085		
[29]		14	0.6247		14	0.5176	81.64	
	IWO	18	0.1049	57.47	18	0.1147		
		32	1.0560		32	1.0842		

4. CONCLUSION

This paper has presented a methodology of fine-tuned PSO technique to obtain the optimal location and sizing of different type of DGs in a radial distribution network. Type I DGs with unity PF and type II DGs with 0.9 PF were used for the integration to the system. The study presented, demonstrates how type II DGs are effective on enhancement in loss reduction and voltage stability of the network system. It was revealed that the proposed fine-tuned PSO performs better in comparison with other methods of optimization for the placement and sizing problems of distributed generators.

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