GWO Based Optimal Reactive Power Coordination of DFIG, ULTC and Capacitors

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Article Info	ABSTRACT				
Article history: Received Mar 6, 2018 Revised Apr 28, 2018 Accepted Jun 10, 2018 Keywords: Doubly Fed Induction Generator (DFIG) Grey Wolf Optimization Algorithm (GWO) On Load Tap Changer (ULTC)	Wind is available with free of cost anywhere in the world, this wind can be used for power generation due to many advantages. This attracts the researchers to work on wind power plants. The presence of wind power plants on distribution system causes major influence on voltage controlled devices (VCDs) in terms of life of the devices. Therefore, this paper proposes grey wolf optimization method (GWO) together with forecasted load one day				
	in advance. VCDs are on load tap changer (ULTC) and capacitors (CS), there are two main objectives first one is curtail of distribution network (DN) loss and second one is curtailing of ULTC and CS switching's. Objectives are achieved by controlling the reactive power of DFIG in coordination with VCDs. The proposed method is planned and applied in Matlab/Simulink on 10KV practical system with DFIG located at different locations. To validate the efficacy of GWO, results are compared with conventional and dynamic programming methods without profane grid circumstances.				
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1. INTRODUCTION

Today the entire world focusing on Distributed generation because of non availability of input sources for conventional power generating stations and too many advantages of distributed generation (DG). Wind power is one of the best sources in DG, this attracts the research people to work on this [1]. In [2-3], Co-Evolutionary particle swarm algorithm and Artificial immune system are proposed for optimal placement and sizing of DGs. DGs are affecting the voltage stability of distribution [4-5]. These papers focused only on optimal placement and impact on voltage stability in the presence of DGs. Generally these DGs are directly connected to distribution system, which influences the power loss and switching operations of ULTC and capacitors, therefore the useful life of these devices are decreasing [6]. In [7] VCDs (ULTC & CS), DG and automatic voltage regulator (AVR) are coordinated, which reported that because of DG the switching operations of devices (SODs) are greatly increased almost more than three times as compared with without DG. SODs are increased more than two times, when VCDs and DG coordinated by SCADA system [8]. In [9-10] VCDs are coordinated using two different approaches, first one is dynamic programming and second one is combined voltage control. In all these methods DGs are not included while dispatching the reactive power.

In [11], synchronous machine as a DG and this reactive power is coordinated in the presence of VCDs. In [12], an autonomous system is taken including DG and real power of DG is coordinated together with power loss by optimal power flow approach. In [13-17], coordination done by TRSQP method, asynchronous and synchronous generators coordinated together with VCDs by voltage control, adaptive and

dynamic programming approaches are used for coordination respectively. All these methods are giving more importance for dispatchable DGs and the importance given for non dispatchable DGs are very small.

The objectives of this paper are reduction of power loss and switching operations of VCDs in the presence of DFIG. This can achieve by coordinating the reactive power DFIG and VCDs. This paper proposes grey wolf optimizer algorithm for reactive power coordination of DFIG, ULTC and Shunt capacitors in order to reduce power loss and switching operations of ULTC and Shunt capacitors.

2. MATHEMATICAL MODELLING OF DFIG

Mathematical modelling of DFIG is very important, which affects the output of DFIG and therefore losses and SODs. Input to DFIG is wind, which is not constant throughout a day or hour, so, the output of DFIG also changes. In mathematical modelling a relation is developed between input and output in terms of probability density function (PDF). This PDF describes the availability of wind based on that we can est imate the output of DFIG [18]. In generally wind speed of wind farm nearly similar to weibull distribution for particular time at a particular location [19]. Now the PDF can be written as:

$$PDF(vel) = \frac{SF}{SCF} \times \left(\frac{vel}{SCF}\right)^{SF-1} \times \exp^{-(vel \times SCF)^{SF}}$$
(1)

$$WPDF(vel) = 1 - \exp^{-\left(\frac{vel}{SCF}\right)^{SF}}$$
(2)

In Equations 1 & 2, PDF(vel), WPDF(vel), SF, SCF, vel, exp, denotes probability density function, weibull PDF, shape factor, scale factor, wind velocity and exponential respectively.

Based on Equations 1 & 2 the output of DFIG is characterised into three parts based on wind velocity. If wind speed is below cut in speed and above cut off speed the output of DFIG is taken as '0'. If wind speed is above cut in and below rated the output of DFIG is written as $0.5 \times AD \times (RRB)^2 \times MPC \times (vel)^3$. In remaining cases output is written as RP. Where AD, RRB MPC and RP represents air density, rotor blade radius, maximum coefficient related to performance and rated power respectively. Figure 1 shows the power availability of DFIG with respect to speed [20-21]. Figure 2 shows single line diagram of system with distributed generation.

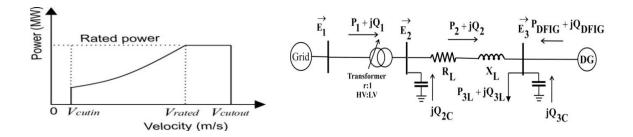


Figure 1. DFIG output characteristic

Figure 2. Single line diagram of system with distributed generation

3. PROBLEM FORMULATION

There are two main objectives of this paper; first one is reduction of SODs and second one is system power loss reduction. The objective function is modelled as a multi objective function; Figure 2 is used for this purpose.

Where E represents voltage, suffix 1 represents grid, suffix 2 and 3 indicates sending and receiving ends respectively, suffix DFIG indicates DG as a DFIG, P & Q indicates real power and reactive power respectively. R_L And X_L indicates line resistance and reactance, suffix 2C and 3C indicates capacitor at sending end and receiving end respectively.

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The first objective, power loss is shown in Equation 3 is written by taking receiving end voltage as a reference. Power loss of the line is proportional to current and line resistance, therefore power loss can be written as:

$$P_{LL}^{h} = I_{L}^{2} \times R_{L}$$
⁽³⁾

After substituting the value of current in terms of sending end voltage and receiving end voltage, the power loss equation is writer as:

$$P_{LL}^{h} = \left| \frac{E_2 \times \cos(\delta) + jE_2 \times \sin(\delta) - E_3}{R_L + jX_L} \right|^2 \times R_L$$
(4)

The second objective is written by considering one ULTC with a tap of r' and two capacitors one is at sending end another is at receiving end:

$$SODs^{h} = f(tap, capacitor)$$
⁽⁵⁾

Generally capacitors at sending end and receiving end are more than one in number. Objective function is expressed as:

$$OBF = P_{IL}^h + SODs^h \tag{6}$$

Where h' stands for hour, power loss and SODs are multiplied with cost weighting factors to get general multi objective function. The multi objective function is written as;

$$OBE = \min \sum_{h=1}^{24} \left(CP \times P_{LL}^{h} + C_1 \times \left| r^{h} - r^{h-1} \right| + C_2 \times \left| K_{Sb}^{h} - K_{Sb}^{h-1} \right| + C_3 \times \left| K_{Fc}^{h} - K_{Fc}^{h-1} \right| \right)$$
(7)

Constraints are listed in the following way: Equality constraints

$$P_{DG} - P_L = P_{Loss} \tag{8}$$

$$Q_{DG} - Q_L = Q_{Loss} \tag{9}$$

Inequality constraints

$$Q_{DG}^{\min} \le Q_{DG} \le Q_{DG}^{\max} \tag{10}$$

$$E^{\min} \le E \le E^{\max} \tag{11}$$

$$r^{\min} \le r \le r^{\max} \tag{12}$$

$$K_{Sc}^{\min} \le K_{Sc} \le K_{Sc}^{\max} \tag{13}$$

$$K_{Fc}^{\min} \le K_{Fc} \le K_{Fc}^{\max} \tag{14}$$

Here *CP*, C_1 , C_2 , and C_3 are the cost weighting factor for power loss, ULTC, substation capacitors and feeder capacitors respectively. K_{Sc} and K_{Fc} are indicating number of capacitors at substation and feeders respectively.

4. GREY WOLF OPTIMIZER ALGORITHM (GWO)

The multi objective function formulated and indicated in equation 3 requires qualitative algorithm for generating the best result among different combinations. Too many algorithms are available like evolutionary based, SI based and physics based. Among evolutionary Genetic algorithm is most powerful and best algorithm proposed in 1992 [22-23]. The remaining some of the important algorithms under this group are differential evolution, evolutionary programming and strategy [24-25]. Some of the important physics based algorithms are GLSA [26], BBBC [27], GSA [28], and ACROA [29], in the SI group the important algorithms are terminate algorithm (TA) [30], Bee collecting pollen algorithm (BCPA) [31], Monkey search algorithm (MS) [32] and Wasp swarm algorithm (WSA) [33].

The algorithms listed above inspired by exploration and hunting behaviours, there is no algorithm which apes both the behaviours in leadership hierarchy, therefore this paper proposes GWO algorithm [34] for solving multi objective function, which ape hunting, exploration in a leadership hierarchical. This algorithm follows three major steps, first step involves look, pursue and move towards the quarry. Second step involves chase, surround and hassle the quarry. Third step involves hitting the quarry.

4.1. GWO Implementation to Objective Function

Implementation of GWO algorithm is as follows:

Step 1: Set all initial conditions.

The values of cost weighting factors CP, C_1 , C_2 and C_3 , number of searching agents, maximum

iterations, number of parameters to be tuned and their minimum and maximum limits, initial values for alpha, beta and delta, forecasted load.

- Step 2: Calculate power loss in the system for first hour Run Backward/Forward algorithm with initial values and calculate power loss and voltages at all the buses in the system.
- Step 3: Calculate Objective function value of each search agent

With obtained power loss in step 2, with initial values of parameters and their cost weighting factors calculate objective function value of each search agent.

Step 4: Update voltages

Run Backward/Forward algorithm with updated search agents and update all buses voltages.

Step 5: Fitness function calculation

Calculate the fitness function value using equation 2.

Step 6: Update alpha, beta and delta

If fitness value is less than alpha score then update alpha with alpha score is equal to fitness, if fitness is greater than alpha score but less than beta score update beta with beta score is equal to fitness, if fitness is greater than alpha score and beta score but less than delta score then update delta with delta score is equal to fitness value.

Step 7: Update positions of search agents including omega

Generate two random numbers Rn1, Rn2 and then evaluate matrix B & C using the following equations 15-16, update the distance of each search agent with the help of equations 17-20.

$$B = 2 \times a \times Rn1 - a \tag{15}$$

$$F = 2 \times Rn2 \tag{16}$$

$$D_{alpha} = F \times P_{alpha} - Best_{alpha} \tag{17}$$

$$D_{beta} = F \times P_{beta} - Best_{alpha} \tag{18}$$

$$D_{delta} = F \times P_{delta} - Best_{alpha} \tag{19}$$

$$D_{omega} = F \times P_{omega} - Best_{alpha} \tag{20}$$

Where P indicates present position, D indicates distance and Best indicates present best position. Step 8: Update parameters to be tuned

Based on the positions of search agents update the parameters which are to be determined.

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Step 9: Update voltages

Run Backward/Forward algorithm with updated search agents and update all buses voltages.

Step 10: Repeat steps 2 to 9 for remaining hours

In this paper the total time is spatter into 24 hours, therefore, repeat the same procedure using steps 2 to 9.

Step11: Stopping criteria

If iterations are completed then stop and display best results in every hour.

5. TEST SYSTEM

10KV practical system which is used for testing purpose is shown in Figure 3. This system consists of 16 buses or nodes, one transformer with 32 steps ULTC, four groups of capacitor banks, three feeders and loads at all buses other than bus 16 & 1. Transformer is 40MVA, 70/10KV rating, one capacitor bank with three capacitors each 2.5MVAR rated is connected at bus 1, second capacitor bank with five capacitors each with a rating of 1.5MVAR connected at bus 4, third capacitor bank with five 1.5MVAR capacitors connected at bus 9 and fourth capacitor bank with four 1.5MVAR capacitors are connected at bus 13.

In order to reduce the power loss and SODs, the load is forecasted one day in advance and is shown in Table 1. In this table only real power for 24 hours at all the buses are indicated, from the real power we can find the reactive power at each bus by taking its power factor. The power factor of all loads is taken as 0.8 lagging. Figure 4 shows the expected real power of DFIG over 24 hours time from this reactive power is estimated by taking power factor of 0.9lag/lead.

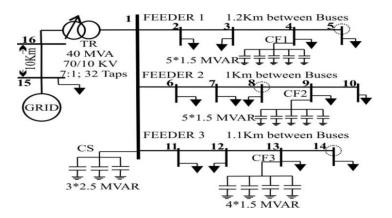


Figure 3. 10KV test system

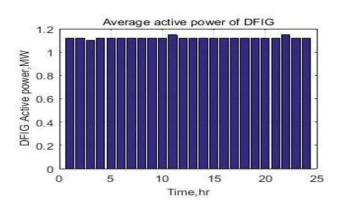


Figure 4. DFIG expected real power over 24 hours

Table 1. Forecasted Load Over 24 Hours																
Feeder Bus numbers																
Hours	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
1	0.0	1.0	1.0	0.6	0.7	0.6	0.4	0.8	0.4	0.8	1.1	1.3	1.6	1.6	5.0	0.0
2	0.0	1.0	0.7	0.4	0.8	0.2	0.1	0.4	0.2	0.4	1.3	1.5	1.4	1.6	5.0	0.0
3	0.0	0.6	0.5	0.3	0.4	0.1	0.3	0.2	0.3	0.6	1.2	1.4	1.6	1.3	5.0	0.0
4	0.0	0.3	0.7	0.2	0.3	0.5	0.5	0.6	0.7	0.8	1.4	1.2	1.7	1.7	5.0	0.0
5	0.0	0.6	0.6	0.7	0.9	1.1	0.7	0.8	0.9	0.8	1.3	1.3	1.6	1.8	5.0	0.0
6	0.0	1.7	1.7	1.3	1.2	1.2	0.9	0.7	1.1	1.0	1.2	1.1	1.5	1.4	5.0	0.0
7	0.0	1.8	1.8	1.8	1.9	1.5	1.2	0.9	1.1	0.8	1.1	0.7	1.0	0.8	5.0	0.0
8	0.0	2.0	2.2	2.0	2.1	1.6	1.4	1.3	1.2	0.9	0.9	0.9	0.9	0.9	5.0	0.0
9	0.0	2.1	2.3	2.1	2.4	1.6	1.6	1.5	1.9	1.8	0.7	0.8	1.0	0.9	5.0	0.0
10	0.0	2.6	2.2	2.3	2.9	2.1	2.0	2.1	1.8	1.9	1.5	1.1	1.2	1.3	5.0	0.0
11	0.0	2.9	2.7	2.8	3.2	2.0	2.3	2.5	2.0	2.1	1.8	1.7	1.4	1.6	5.0	0.0
12	0.0	2.2	2.1	2.7	1.9	1.4	1.9	2.2	1.6	1.9	1.2	1.4	1.3	1.4	5.0	0.0
13	0.0	2.9	2.9	3.0	3.2	2.3	2.9	3.0	2.4	2.1	1.5	1.6	1.8	1.4	5.0	0.0
14	0.0	3.1	3.2	3.5	3.3	2.7	3.1	3.0	2.7	1.2	1.7	1.8	1.8	1.4	5.0	0.0
15	0.0	3.0	3.0	3.4	3.2	2.6	2.9	3.0	2.4	1.1	1.5	1.6	1.9	1.6	5.0	0.0
16	0.0	2.7	2.9	3.3	3.0	2.5	2.8	1.7	1.7	1.5	1.6	1.8	2.1	1.8	5.0	0.0
17	0.0	3.1	3.2	3.1	2.9	2.4	2.3	2.2	2.3	1.8	2.0	1.8	2.1	1.8	5.0	0.0
18	0.0	2.5	2.7	2.9	2.4	2.4	2.1	1.8	1.8	1.2	1.9	2.1	2.0	2.2	5.0	0.0
19	0.0	2.0	2.0	2.0	1.8	1.8	1.4	1.3	1.2	1.3	1.9	2.1	2.0	2.2	5.0	0.0
20	0.0	1.6	1.6	1.8	1.7	1.4	1.3	1.3	1.1	1.3	1.9	2.0	1.5	1.5	5.0	0.0
21	0.0	1.6	1.4	1.7	1.5	1.3	1.4	1.2	1.1	1.2	1.8	1.9	1.5	1.4	5.0	0.0
22	0.0	1.2	1.3	1.4	1.2	0.6	0.9	1.1	1.2	1.1	1.8	1.7	1.8	1.3	5.0	0.0
23	0.0	1.2	1.0	1.3	1.1	0.5	0.6	1.3	0.8	1.2	1.6	1.6	1.8	1.7	5.0	0.0
24	0.0	1.0	0.9	0.6	0.9	0.5	0.2	0.8	0.6	1.2	1.7	1.7	1.6	1.1	5.0	0.0

6. **RESULTS & DISCUSSION**

Test system shown in Figure 4 is simulated with load shown in Table 1 and DG output shown in Figure 5. DG is placed at three different locations and in each location the simulation results are listed in Tables 2 to 4. Conventional method represents power loss of 13.69MWh, ULTC is changing 6 times, substation capacitors are changing 14 times, capacitors at feeder 1 changes 10 times and capacitors at feeder 2 and 3 changes 10 times and six times respectively with DG connected at bus 5 in feeder 1. If DG is connected to feeder 2 at bus 8, conventional method reported that 13.9MWh power loss, 6 times ULTC variations, 14 times substation capacitors variations, 10 variations in feeder 1 capacitors, 10 variations in feeder 2 capacitors and 6 variations in feeder 3 capacitors. In similarly power loss, ULTC and Capacitor variations are shown in Table 4. In conventional method DG is operating at unity power factor, therefore, power loss and SODs are more.

Simulation results with dynamic programming (DP) are reported in Tables 2 to 4. In Table 2, 13.67MWh is the power loss; there are 6 changes in ULTC, 12, 8, 6, 4 changes in substation capacitors, feeder 1 capacitors, feeder 2 capacitors and feeder 3 capacitors respectively. From Table 3, 13.83MWh power loss; 6, 12, 10, 8, 4 variations in ULTC, substation capacitors, feeder 1 capacitors, feeder 2 capacitors and feeder 3 capacitors, feeder 1 capacitors, feeder 2 capacitors and feeder 3 capacitors are noted respectively. Similarly DG at 14 results is shown in Table 4. In dynamic programming method reactive power of the DG is considered [16]. Results with grey wolf optimizer are reported in Tables 2 to 4 with DGs at 5, 8 and 14 respectively. From the results listed in Tables 2 to 4, reactive power of DG is properly utilized by GWO method as compared with Dynamic programming and conventional methods (CO).

DG at 5, GWO reduces power loss by 2.0606MWh as compared with conventional and 2.0406MWh as compared with DP, ULTC switching operations are also reduced by 4 times compared with CO and DP, substation capacitor switching operations reduced by 14 and 12 times compared with CO and DP respectively, feeder capacitors switching operations are reduced by 21 times and 13 times compared with CO and DP. DG at 8, GWO reduces power loss by 3.5105MWh as compared with conventional and 3.4405MWh as compared with DP, ULTC switching operations are also reduced by 4 times compared with CO and DP, substation capacitor switching operations reduced by 12 and 10 times compared with CO and DP, substation capacitor switching operations are reduced by 19 times and 15 times compared with CO and DP. DG at 14, GWO reduces power loss by 3.1191MWh as compared with conventional and 3.0591MWh as compared with DP, ULTC switching operations are also reduced by 14 and 12 times compared with CO and DP. DG at 14, GWO reduces power loss by 3.1191MWh as compared with conventional and 3.0591MWh as compared with DP, ULTC switching operations are also reduced by 14 and 12 times compared with CO and DP. DG at 14, GWO reduces power loss by 3.1191MWh as compared with conventional and 3.0591MWh as compared with DP, ULTC switching operations are also reduced by 5 times compared with CO and DP respectively, feeder capacitor switching operations reduced by 14 and 12 times compared with CO and DP respectively, feeder capacitor switching operations are reduced by 25 times and 21 times compared with CO and DP respectively, feeder capacitors switching operations are reduced by 25 times and 21 times compared with CO and DP.

Table 5 reports the cost comparison of three methods with DG at 5, 8 and 14 locations. Cost of power loss, switching loss and total are calculated using the equations 21 to 23. From this table, DP method

reduced power loss by 0.146% and GWO method reduced power loss by 15.05% as compared with CO method, switching operations of VCDs are reduced by 18.64% in DP and 84.745% in GWO compared with CO and also total cost reduced by DP is 12.78% and GWO by 62.65% in comparison with CO if DG is located at 5. If DG is located 8, DP reduces power loss, switching operations of VCDs and total power loss by 0.5035%, 11.864% and 8.225% respectively compared with CO, GWO reduces power loss, switching operations of VCDs and total power loss by 25.2554%, 74.576% and 58.779% respectively compared with CO. If DG at 14, DP reduces power loss, switching operations of VCDs and total power loss by 0.4264%, 11.475% and 7.987% respectively compared with CO, GWO reduces power loss, switching operations of VCDs and total power loss by 22.168%, 91.80% and 69.82% respectively compared with CO.

$$Powerlos(\$) = 80 \times powerlos(MWh)$$
(21)

$$Switchingdss(\$) = 80*ULTC + 60*CS + 40*(CF1 + CF2 + CF3)$$
(22)

$$Totallos(\$) = Powerlos(\$) + Switchingdss(\$)$$
(23)

	Table 2. DG Located at Bus 5									
DG Loca	tion		At Bus 5							
Control M	ethods	Conventional	Dynamic programming	Grey wolf optimizer						
Power loss	Power loss (MWh)		13.67	11.6294						
	ULTC	6	6	2						
Switching	CS	14	12	0						
operations			8	2						
of VCDs	CF2	10	6	2						
	CF3	6	4	1						
Power loss (\$)		1095.2	1093.6	930.352						
Switching Loss(\$)		2360	1920	360						
Total Lo	ss(\$)	3455.2	3013.6	1290.352						

Table 3. DG Located at Bus 8

DG Loca	ation		At Bus 8			
Control M	ethods	Conventional	Dynamic programming	Grey wolf optimizer		
Power loss	(MWh)	13.90	13.83	10.3895		
	ULTC		6	2		
Switching	CS	14	12	2		
operations	CF1	10	10	3		
of VCDs	CF2	10	8	1		
	CF3	6	4	4		
Power los	Power loss (\$)		1106.4	831.16		
Switching I	Switching Loss(\$)		2080	600		
Total Lo	ss(\$)	3472	3186.4	1431.16		

Table 4. DG Located at Bus 14

DG Loca	ation		At Bus 14	
Control M	Control Methods		Dynamic programming	Grey wolf optimizer
Power loss	Power loss (MWh)		14.01	10.9509
	ULTC		6	1
Switching	CS	14	12	0
operations	CF1	10	10	1
of VCDs	CF2	10	8	1
CF3		8	6	1
Power loss (\$)		1125.6	1120.8	876.072
Switching Loss(\$)		2440	2160	200
Total Lo	oss(\$)	3565.6	3280.8	1076.072

Table 5. Cost Comparison of Different Algorithms										
DG location		At 5		At 8				At 14		
Control Methods	CO	DP	GWO	CO	DP	GWO	CO	DP	GWO	
Power loss (\$)	1095.2	1093.6	930.352	1112	1106.4	831.16	1125.6	1120.8	876.072	
Switching Loss(\$)	2360	1920	360	2360	2080	600	2440	2160	200	
Total Loss(\$)	3455.2	3013.6	1290.352	3472	3186.4	1431.16	3565.6	3280.8	1076.07	
Power loss comparison (\$)		0.1460	15.051		0.503	25.255		0.426	22.168	
Switching Loss comparison (\$)		18.644	84.745		11.864	74.576		11.475	91.803	
Total cost comparison (\$)		12.780	62.654		8.225	58.779		7.987	69.82	

7. CONCLUSION

The following conclusions are derived based on the results:

a. Power loss reduction: proposed method reduced power loss maximum by 25.2554% and minimum by 15.05% compared with conventional and 24.88% maximum and 14.93% minimum compared with DP.

b. Switching loss: proposed method reduced switching loss maximum by 91.80% and minimum by 74.57% compared with conventional and 90.74% maximum and 71.15% minimum compared with DP.

c. Total loss: proposed method reduced total loss maximum by 69.82% and minimum by 58.78% compared with conventional and 67.20% maximum and 55.08% minimum compared with DP.

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